

INTERNAL REPORTS IN  
SIMULATION, OPTIMIZATION  
AND CONTROL

No. SOC-191

SUBROUTINES FOR IMPLEMENTING QUADRATIC  
MODELS OF SURFACES IN OPTIMAL DESIGN

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April 1978

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SUBROUTINES FOR IMPLEMENTING QUADRATIC MODELS OF  
SURFACES IN OPTIMAL DESIGN

H.L. Abdel-Malek and J.W. Bandler

Abstract

This collection of subroutines is primarily for approximating functions of many variables by quadratic polynomials as well as evaluating them. They are oriented for use in a tolerance optimization process. The quadratic approximation is obtained, exploiting sparsity, in Subroutine MODEL4. The evaluation of the resulting polynomial at the vertices of the tolerance orthotope is performed using an efficient technique.

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This work was supported by the National Research Council of Canada under Grant A7239 and by a Postdoctorate Fellowship to H.L. Abdel-Malek.

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DESCRIPTION

This report should be read in conjunction with previous work by the authors [1-3]. The quadratic interpolation is performed by solving a system of linear equations with the coefficients of the quadratic polynomial as unknowns. In general, the resulting system of linear equations is of order

$$N = (k+1)(k+2)/2,$$

where  $k$  is the number of parameters [1].

For a particular choice of base points (points where the quadratic polynomial coincides with the approximated function), the effort in solving the system of simultaneous linear equations can be reduced to  $5k^2 - 2k$  operations (multiplications or divisions) instead of the well known  $(N^3 + 3N^2 - N)/3$  operations for Gauss elimination. This is done by exploiting sparsity in the system of linear equations in Subroutine MODEL4.

The evaluation of the quadratic polynomial and its derivatives using Subroutine QPE is performed in an efficient manner. The procedure is to start by evaluating the polynomial and its derivatives at the vertex nearest to the origin. Values at other vertices are obtained from neighbouring ones exploiting simple properties of quadratic polynomials [1,2].

Subroutine VERT generates the vectors  $\underline{\mu}^r$  for each vertex  $\phi^r$  [1,2], according to the vertex numbering scheme

$$r = 1 + \sum_{i=1}^k \left( \frac{\mu_i^{r+1}}{2} \right) 2^{i-1} .$$

REFERENCES

- [1] J.W. Bandler and H.L. Abdel-Malek, "Optimal centering, tolerancing and yield determination using multidimensional approximations", Proc. 1977 IEEE Int. Symp. Circuits and Systems (Phoenix, AZ, April 1977), pp. 219-222.
- [2] J.W. Bandler and H.L. Abdel-Malek, "Optimal centering, tolerancing and yield determination via updated approximations and cuts", Faculty of Engineering, McMaster University, Hamilton, Canada, Report SOC-173, June 1977 (Revised Dec. 1977).
- [3] H.L. Abdel-Malek and J.W. Bandler, "Yield optimization for arbitrary statistical distributions", Proc. 1978 IEEE Int. Symp. Circuits and Systems (New York, NY, May 1978).

APPENDIX

FORTRAN LISTING OF THE SUBROUTINES MODEL4, QPE AND VERT



|    |  |          |
|----|--|----------|
| C  |  | MOD 740  |
| C  |  | MOD 750  |
|    | DIMENSION X(N), B(NOBP, NR), V(NREM), CX(N), AF(NR), TAF(NR) | MOD 760  |
|    | DIMENSION H(N)   | MOD 770  |
| C  |  | MOD 780  |
|    | IF(IJ.EQ.0) GO TO 10   | MOD 790  |
|    | MM=((N+2)*(N+1))/2   | MOD 800  |
|    | MM1=MM-1   | MOD 810  |
|    | MMN=MM-N-1   | MOD 820  |
|    | LK=N-1   | MOD 830  |
| 10 | CALL SECOND(T1)  | MOD 840  |
|    | DO 20 J=1, N   | MOD 850  |
|    | CX(J)=X(J)   | MOD 860  |
| 20 | CONTINUE   | MOD 870  |
|    | CALL ACFUNS(X, AF)   | MOD 880  |
|    | DO 25 J=1, NR  | MOD 890  |
|    | B(MM, J)=AF(J)   | MOD 900  |
|    | TAF(J)=AF(J)+AF(J)   | MOD 910  |
| 25 | CONTINUE   | MOD 920  |
|    | DO 40 I=1, N   | MOD 930  |
|    | X(I)=CX(I)+H(I)  | MOD 940  |
|    | CALL ACFUNS(X, AF)   | MOD 950  |
|    | DO 30 J=1, NR  | MOD 960  |
|    | B(I, J)=AF(J)  | MOD 970  |
| 30 | CONTINUE   | MOD 980  |
|    | X(I)=CX(I)-H(I)  | MOD 990  |
|    | CALL ACFUNS(X, AF)   | MOD 1000 |
|    | TH=H(I)+H(I)   | MOD 1010 |
|    | HH=H(I)*H(I)   | MOD 1020 |
|    | THH=HH+HH  | MOD 1030 |
|    | DO 35 J=1, NR  | MOD 1040 |
|    | B(MMN+I, J)=(B(I, J)-AF(J))/TH                               | MOD 1050 |
|    | B(I, J)=(B(I, J)+AF(J)-TAF(J))/THH                           | MOD 1060 |
| 35 | CONTINUE   | MOD 1070 |
|    | X(I)=CX(I)   | MOD 1080 |
| 40 | CONTINUE   | MOD 1090 |
|    | IR=N   | MOD 1100 |
|    | IRR=1  | MOD 1110 |
|    | DO 50 I=1, LK  | MOD 1120 |
|    | I1=I+1   | MOD 1130 |
|    | MI=MMN+I   | MOD 1140 |
|    | DO 50 K=I1, N  | MOD 1150 |
|    | VHI=V(IRR)*H(I)  | MOD 1160 |
|    | VHK=V(IRR+1)*H(K)  | MOD 1170 |
|    | MK=MMN+K   | MOD 1180 |
|    | IR=IR+1  | MOD 1190 |
|    | IRR=IRR+2  | MOD 1200 |
|    | X(I)=CX(I)+VHI   | MOD 1210 |
|    | X(K)=CX(K)+VHK   | MOD 1220 |
|    | DV=VHI*VHK   | MOD 1230 |
|    | CALL ACFUNS(X, AF)   | MOD 1240 |
|    | DO 45 J=1, NR  | MOD 1250 |
|    | B(IR, J)=(AF(J)-B(MM, J)-VHI*(VHI*B(I, J)+B(MI, J))          | MOD 1260 |
|    | + -VHK*(VHK*B(K, J)+B(MK, J)))/DV                            | MOD 1270 |
| 45 | CONTINUE   | MOD 1280 |
|    | X(I)=CX(I)   | MOD 1290 |
|    | X(K)=CX(K)   | MOD 1300 |
| 50 | CONTINUE   | MOD 1310 |
|    | DO 65 J=1, NR  | MOD 1320 |
|    | DO 55 I=1, N   | MOD 1330 |
|    | MI=MMN+I   | MOD 1340 |
|    | A=B(I, J)*CX(I)  | MOD 1350 |
|    | B(MM, J)=B(MM, J)+CX(I)*(A-B(MI, J))                         | MOD 1360 |
|    | B(MI, J)=B(MI, J)-A-A  | MOD 1370 |
| 55 | CONTINUE   | MOD 1380 |
|    | IR=N   | MOD 1390 |
|    | DO 60 I=1, LK  | MOD 1400 |
|    | MI=MMN+I   | MOD 1410 |
|    | I1=I+1   | MOD 1420 |
|    | DO 60 K=I1, N  | MOD 1430 |
|    | MK=MMN+K   | MOD 1440 |
|    | IR=IR+1  | MOD 1450 |
|    | A=CX(I)*B(IR, J)   | MOD 1460 |
|    | B(MM, J)=B(MM, J)+A*CX(K)                                    | MOD 1470 |



```
B(MI, J)=B(MI, J)-CX(K)*B(IR, J)
B(MK, J)=B(MK, J)-A
60 CONTINUE
65 CONTINUE
CALL SECOND(T2)
C
IF(MP.NE.1) RETURN
WRITE(6, 200)
DO 70 I=1, N
WRITE(6, 250) H(I)
70 CONTINUE
T=T2-T1
WRITE(6, 260) T
DO 150 MA=1, MR
WRITE(6, 270) MA
WRITE(6, 280) (B(I, MA), I=1, MM)
150 CONTINUE
200 FORMAT(1H1, 4X, *STEPS AROUND CENTER OF INTERPOLATION*)
250 FORMAT(4X, E16.8)
260 FORMAT(/, 4X, *MODELING TIME IN SECONDS =*, E16.8)
270 FORMAT(/, 4X, *ER(*, 12, *)*, /, 4X, 6(*-*))
280 FORMAT(5(4X, E16.8), /)
311 FORMAT(5E16.8)
RETURN
END
```

MOD1480  
MOD1490  
MOD1500  
MOD1510  
MOD1520  
MOD1530  
MOD1540  
MOD1550  
MOD1560  
MOD1570  
MOD1580  
MOD1590  
MOD1600  
MOD1610  
MOD1620  
MOD1630  
MOD1640  
MOD1650  
MOD1660  
MOD1670  
MOD1680  
MOD1690  
MOD1700  
MOD1710  
MOD1720



|    |  |                   |
|----|--|-------------------|
|    | IF(LL.EQ.1) GO TO 10                     | QPE 740           |
|    | DO 5 I=1, NN                             | QPE 750           |
|    | Y(I)=X(I)                                | QPE 760           |
| 5  | CONTINUE                                 | QPE 770           |
|    | GO TO 25                                 | QPE 780           |
| C  |  | QPE 790           |
| C  | STARTING AT THE VERTEX Y(I)=X(I)-X(I+NN) | X(I+NN) IS EPS(I) |
|    |  | QPE 800           |
| 10 | DO 20 I=1, NN                            | QPE 810           |
|    | Y(I)=X(I)-X(I+NN)                        | QPE 820           |
| 20 | CONTINUE                                 | QPE 830           |
| 25 | DO 100 K1=1, NAC                         | QPE 840           |
|    | K=1+NV*(K1-1)                            | QPE 850           |
|    | IF(LL.NE.1) K=K1                         | QPE 860           |
|    | S=B(MM, K1)                              | QPE 870           |
|    | DO 30 I=1, NN                            | QPE 880           |
|    | T=B(I, K1)*Y(I)                          | QPE 890           |
|    | S=S+T*Y(I)                               | QPE 900           |
|    | GE(I, K)=T+T                             | QPE 910           |
|    | H(I, I)=B(I, K1)+B(I, K1)                | QPE 920           |
| 30 | CONTINUE                                 | QPE 930           |
|    | KM=NN                                    | QPE 940           |
|    | DO 40 I=1, LK                            | QPE 950           |
|    | LH=I+1                                   | QPE 960           |
|    | DO 40 J=LH, NN                           | QPE 970           |
|    | KM=KM+1                                  | QPE 980           |
|    | T=B(KM, K1)*Y(I)                         | QPE 990           |
|    | S=S+T*Y(J)                               | QPE1000           |
|    | GE(I, K)=GE(I, K)+B(KM, K1)*Y(J)         | QPE1010           |
|    | GE(J, K)=GE(J, K)+T                      | QPE1020           |
|    | H(I, J)=B(KM, K1)                        | QPE1030           |
|    | H(J, I)=H(I, J)                          | QPE1040           |
| 40 | CONTINUE                                 | QPE1050           |
|    | DO 50 I=1, NN                            | QPE1060           |
|    | KM=KM+1                                  | QPE1070           |
|    | S=S+B(KM, K1)*Y(I)                       | QPE1080           |
|    | GE(I, K)=GE(I, K)+B(KM, K1)              | QPE1090           |
| 50 | CONTINUE                                 | QPE1100           |
|    | ER(K)=S                                  | QPE1110           |
|    | IF(LL.NE.1) GO TO 100                    | QPE1120           |
| C  |  | QPE1130           |
| C  | OTHER VERTICES                           | QPE1140           |
|    |  | QPE1150           |
|    | JU=1                                     | QPE1160           |
|    | L=K                                      | QPE1170           |
|    | LG=1                                     | QPE1180           |
|    | MI=K-1                                   | QPE1190           |
|    | DO 90 I=1, NN                            | QPE1200           |
|    | M=MI                                     | QPE1210           |
|    | INN=I+NN                                 | QPE1220           |
|    | EP=X(INN)                                | QPE1230           |
|    | TE=EP+EP                                 | QPE1240           |
|    | DO 70 IR=1, NN                           | QPE1250           |
|    | H(IR, I)=TE*H(IR, I)                     | QPE1260           |
| 70 | CONTINUE                                 | QPE1270           |
|    | EPH=EP*H(I, I)                           | QPE1280           |
|    | DO 80 J=1, JU                            | QPE1290           |
|    | M=M+1                                    | QPE1300           |
|    | L=L+1                                    | QPE1310           |
|    | LG=LG+1                                  | QPE1320           |
|    | ER(L)=ER(M)+TE*GE(I, M)+EPH              | QPE1330           |
|    | DO 80 IR=1, NN                           | QPE1340           |
|    | GE(IR, L)=GE(IR, M)+H(IR, I)             | QPE1350           |
| 80 | CONTINUE                                 | QPE1360           |
|    | JU=JU+JU                                 | QPE1370           |
| 90 | CONTINUE                                 | QPE1380           |
|    | L=K                                      | QPE1390           |
|    | DO 99 II=1, NV                           | QPE1400           |
|    | DO 95 I=1, NN                            | QPE1410           |
|    | J=I+NN                                   | QPE1420           |
|    | GE(J, L)=FLOAT(IV(I, II))*GE(I, L)       | QPE1430           |
| 95 | CONTINUE                                 | QPE1440           |
|    | L=L+1                                    | QPE1450           |
| 99 | CONTINUE                                 | QPE1460           |
|    |  | QPE1470           |

**100 CONTINUE  
RETURN  
END**

**QPE1480  
QPE1490  
QPE1500**

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

SUBROUTINE VERT(IV,NN,NV)  
-----

THIS SUBROUTINE GENERATES THE MUS ACCORDING TO THE COMMON  
NUMBERING SCHEME OF THE VERTICES

NN = NUMBER OF PARAMETERS (INPUT)  
NV = NUMBER OF VERTICES (INPUT)  
IV = ARRAY OF MUS (OUTPUT)

VER 10  
VER 20  
VER 30  
VER 40  
VER 50  
VER 60  
VER 70  
VER 80  
VER 90  
-----  
VER 100  
VER 110  
VER 120  
VER 130  
VER 140  
VER 150  
VER 160  
VER 170  
VER 180  
VER 190  
VER 200  
VER 210  
VER 220  
VER 230  
VER 240  
VER 250  
VER 260  
VER 270  
VER 280  
VER 290  
VER 300

DIMENSION IV(NN,NV)

11=1  
MI=NV  
DO 30 I=1,NN  
IR=0  
IS=-1  
DO 20 J=1,MI  
DO 10 K=1,II  
IR=IR+1  
IV(I,IR)=IS  
10 CONTINUE  
IS=-IS  
20 CONTINUE  
II=II+1  
MI=MI/2  
30 CONTINUE  
RETURN  
END



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April 1978, No. of Pages: 11

Revised:

Key Words: Surface fitting, quadratic approximation, polynomial evaluation

Abstract: This collection of subroutines is primarily for approximating functions of many variables by quadratic polynomials as well as evaluating them. They are oriented for use in a tolerance optimization process. The quadratic approximation is obtained, exploiting sparsity, in Subroutine MODEL4. The evaluation of the resulting polynomial at the vertices of the tolerance orthotope is performed using an efficient technique.

Description: Contains Fortran Listing, user's manual.  
The listing contains 355 cards, of which 164 are comment cards.

Related Work: SOC-118, SOC-173, SOC-182, SOC-184, SOC-185.

Price: \$15.00.

