

**AUTOMATED DIRECT OPTIMIZATION-
DRIVEN ELECTROMAGNETIC DESIGN OF
HIGH-FREQUENCY AND
HIGH-SPEED CIRCUITS**

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ELECTROMAGNETIC DESIGN OF HIGH-FREQUENCY
AND HIGH-SPEED CIRCUITS**

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NSERC Strategic Project Seminar Spring 1996



Milestones

- | | | |
|--------|---|---------|
| Year 1 | formulate mathematical approaches,
acquisition of external software | Apr. 95 |
| | create electromagnetic design benchmark
problems | Oct. 95 |
| Year 2 | further development of mathematical,
circuit-theory and field-theory based
techniques; resolution of specialized
user-oriented features | Apr. 96 |
| | preliminary integration of software with
public domain or proprietary systems to
test user-oriented features; field testing;
prototype available for installations at
collaborating organizations | Oct. 96 |
| Year 3 | continue algorithm development and
testing; workshop for Canadian
participants | Apr. 97 |
| | production testing and promotion of
documented software; arrange
installation at interested Canadian
organizations | Oct. 97 |



Overview of the Presentation

benchmark EM design problems

- double folded stub filter
- attenuator
- HTS filter
- interdigital combline filter
- frequency doubler
- waveguide transformers

user-defined parameterization of arbitrary structures

parallel computing

Space Mapping

EM optimization of 3D structures

work in progress



Previous Work: Challenges of Automated EM Optimization
(Bandler et al., 1993, 1994)

drastically increased analysis time

discrete nature of some EM solvers

continuity of optimization variables

gradient information

interpolation and modeling

integrated data bases

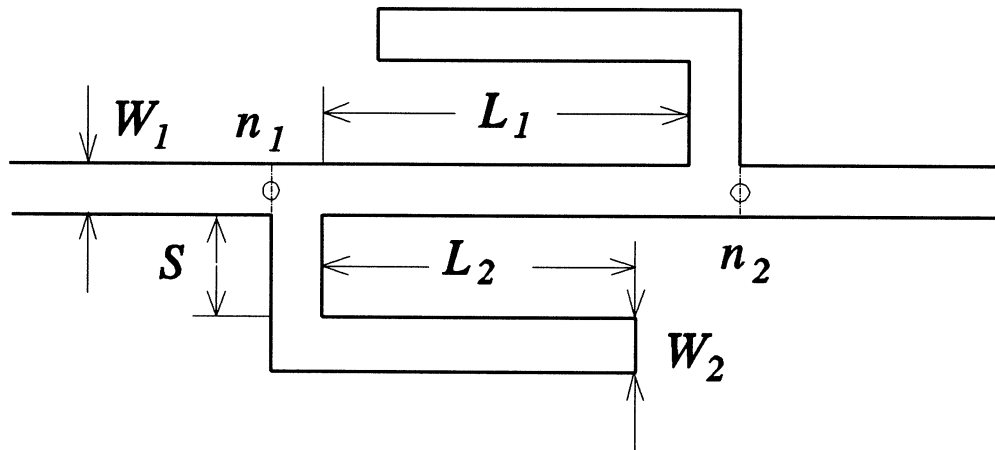
original Space Mapping algorithm



Benchmark EM Design Problems

A Double Folded Stub Filter

(Jim Rautio, Sonnet Software)



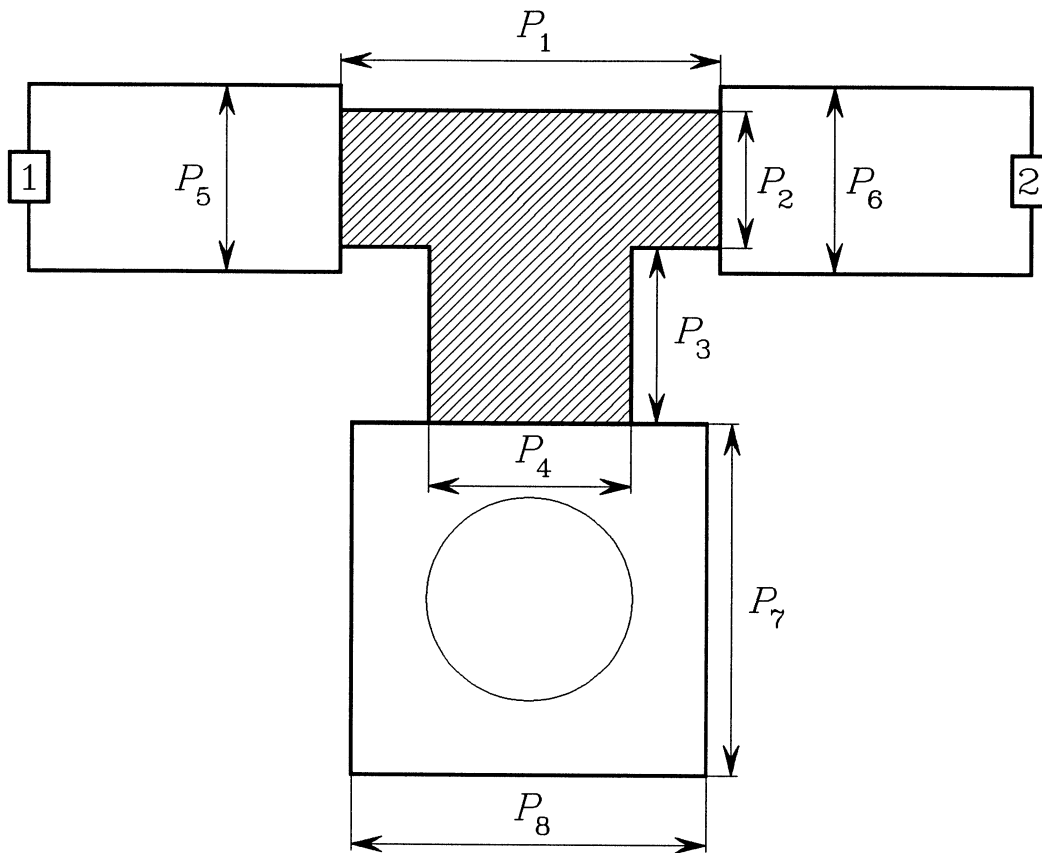
for bandstop filter applications

substantially reduced filter area w.r.t. the conventional double stub structure

substrate thickness is 5 mil and the relative dielectric constant is assumed to be 9.9



Benchmark EM Design Problems
A 10 dB Distributed Attenuator
(Dan Swanson, Watkins-Johnson)



built on a 15 mil thick substrate with relative dielectric constant of 9.8

metallization of a high resistivity ($50 \Omega/\text{sq}$)

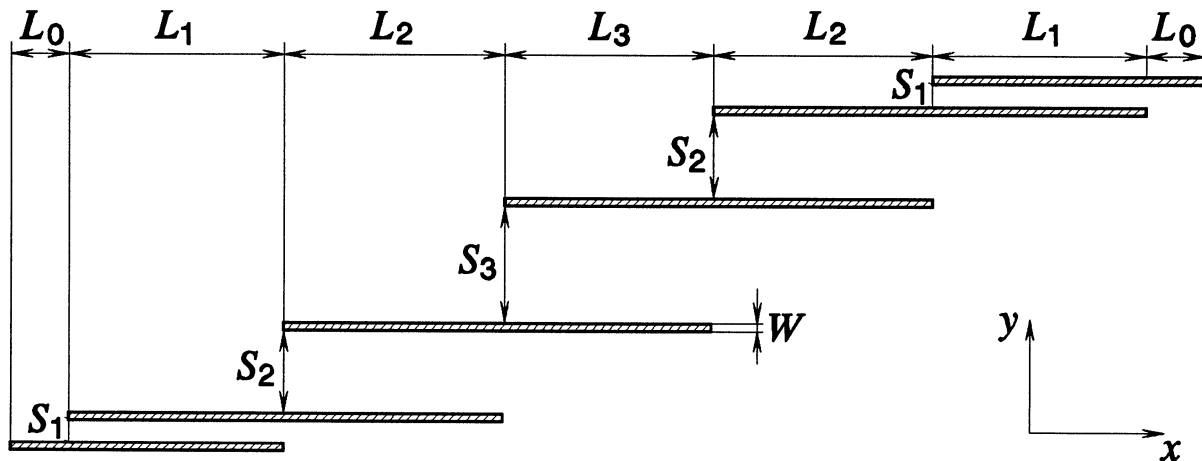
the feed lines and the grounding pad are assumed lossless



Benchmark EM Design Problems

An HTS Filter

(Chuck Moskowitz and Salvador Talisa, Westinghouse)



high-temperature superconducting four pole quarter-wave parallel coupled-line microstrip filter

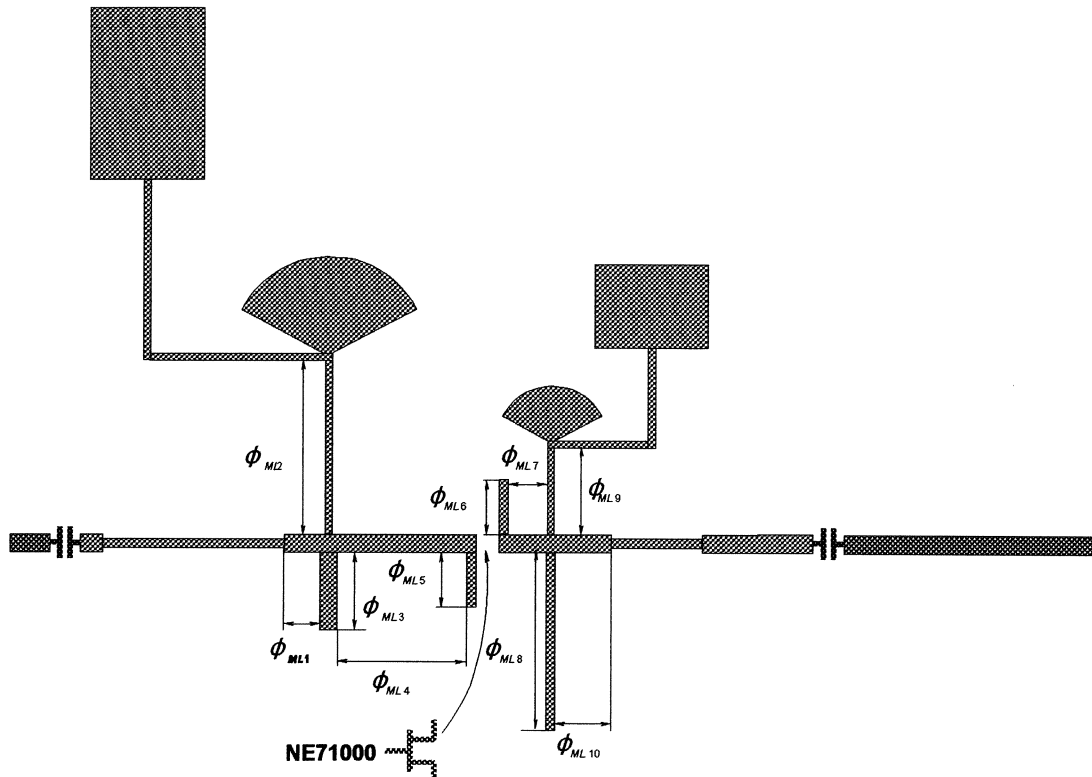
high relative dielectric constant (more than 23) of the substrate material (lanthanum aluminate)

narrow bandwidth (1.25%)



Benchmark EM Design Problems

A Nonlinear FET Class B Frequency Doubler (*Microwave Engineering Europe, 1994*)

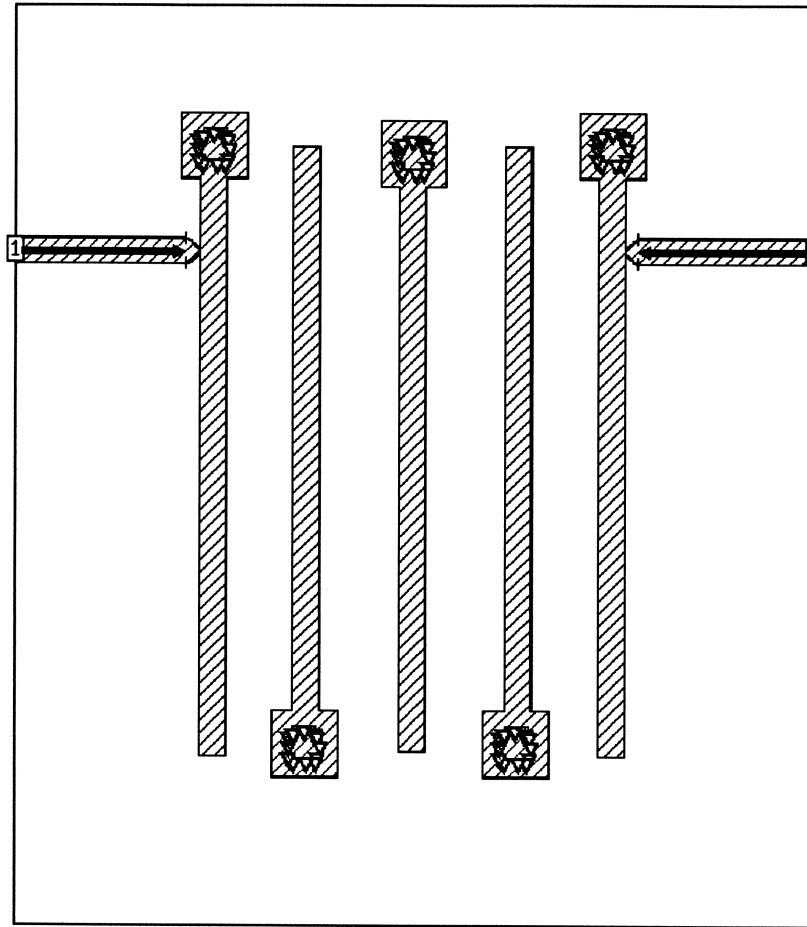


the linear subcircuit is defined as one optimizable structure with 10 variables

requires integration of large-signal harmonic balance of nonlinear circuits with active devices into EM-based optimization



Benchmark EM Design Problems
An Interdigital C-Band Filter
(*Dan Swanson, Watkins-Johnson*)



a five-pole interdigital filter with tapped lines

drawn using *xgeom* of Sonnet Software



User-Defined Parameterization of Arbitrary Structures

to optimize shapes and dimensions of geometrical objects by automatically adjusting the user-defined parameters subject to implicit geometrical constraints

work has included development of theory and algorithms employing concepts from analytic geometry, supported by graphical interfacing

EM simulators deal directly with the layout representation of circuits in terms of absolute coordinates

geometrical coordinates are implicitly related to designable parameters

geometrical parameterization is needed for every new structure

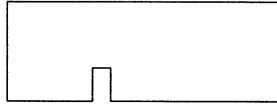
using a graphical layout editing tool the user marks the evolution of the structure as the designable parameters change

a mapping between the geometrical coordinates and the designable parameter values is established

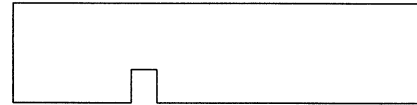
possible extension: establish rules and rule checkers



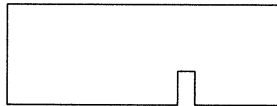
Various Object Evolutions



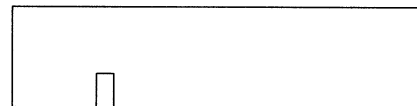
(a)



(b)



(c)

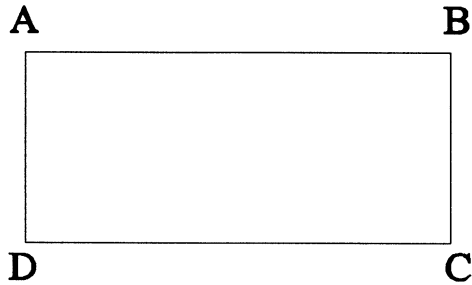


(d)

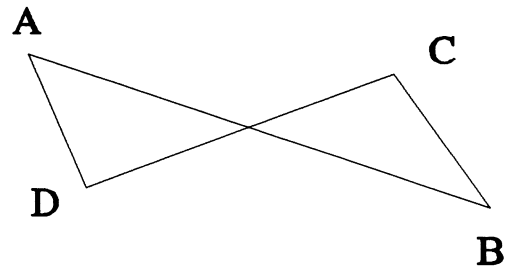
- (a) initial geometry
- (b) proportional expansion of the whole structure along the x axis
- (c) only the location of the slit in the fixed line is allowed to change
- (d) only the segment to the right of the slit is allowed to expand



Possible Pitfalls of Arbitrary Movement of Vertices



(a)



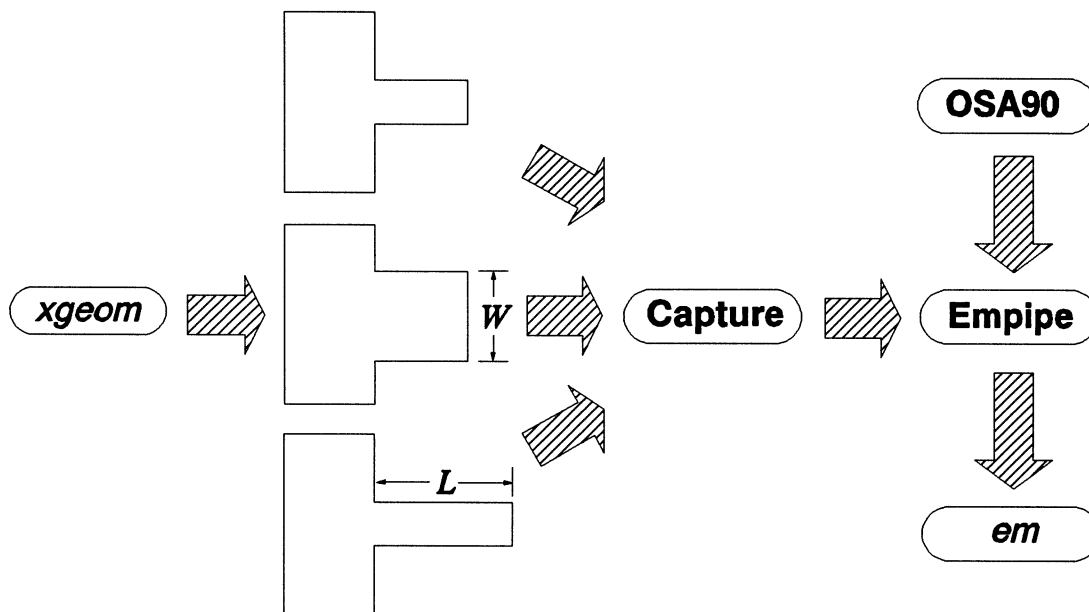
(b)

(a) initial geometry

(b) an unwanted result due to an arbitrary and independent movement of vertices



Implementation of User-Defined Parameterization





Direct EM Optimization of the Frequency Doubler
(Bandler, Biernacki, Cai, Chen and Grobelny, 1995)

involves optimization of an arbitrary planar structure

the complete structure between the two capacitors is considered as a whole and simulated by Sonnet's *em*

Empipe links *em* simulations to the optimizer

the performance of the overall circuit is directly optimized with 10 optimization variables

design specification:

conversion gain > 3 dB
spectral purity > 20 dB

at 7 GHz and 10 dBm input power



Interface to Various CAD Simulators

to expand our interprocess pipe communication (IPPC) technique for integrating simulators into optimization systems

capable of handling any specific syntax of a given simulator

simulation results captured from the output files of those simulators and returned to the optimizer

to be capable of learning the output format of any specific simulator

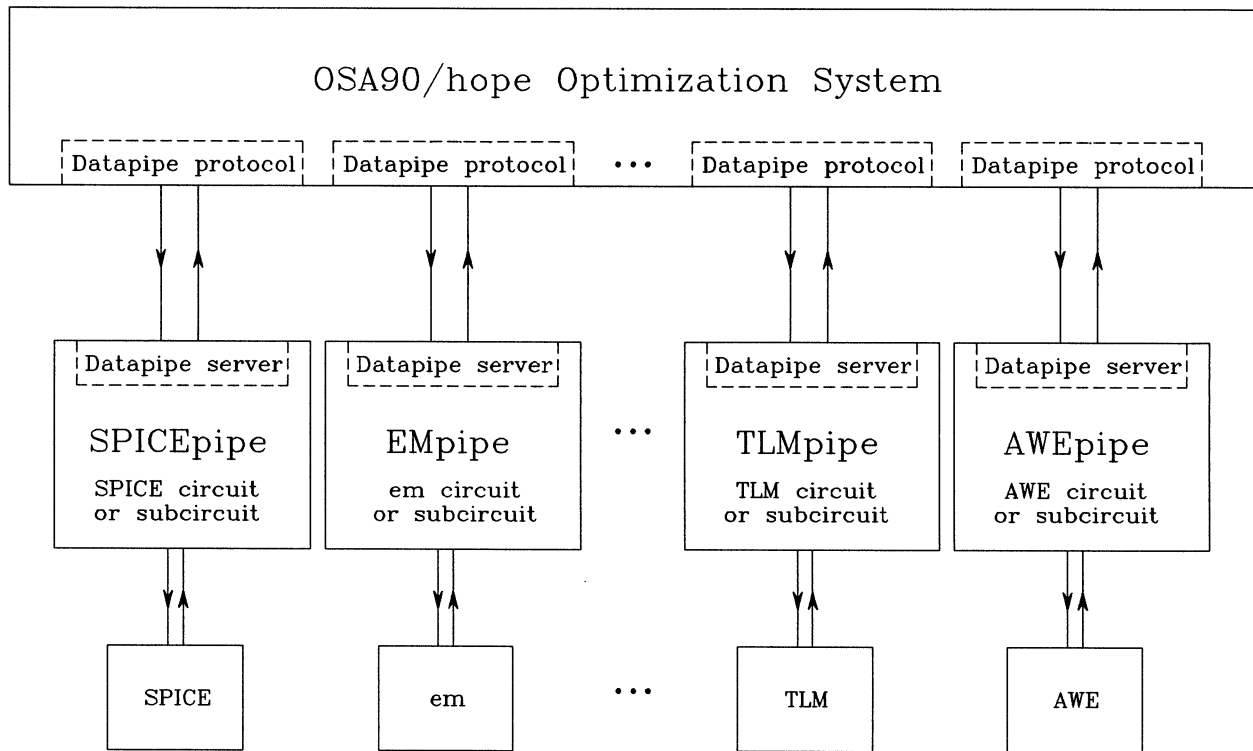
multi-level distributed calculations with design variables defined at different levels

interpolation/modelling capability and database management

parallel computing as an effective means of speeding up CPU intensive EM optimization



Integration of Various CAD Tools





Parallel Computing Options

multiprocessor computers and specialized compilers vs.
distributing EM analyses over a computer network

the overhead of parallelization is negligible as compared to
the CPU-intensive EM analyses

splitting at the component/subcircuit level

suitable when several EM simulation results are needed
simultaneously

- off-grid interpolation

- numerical gradient estimation

- multiple outcomes in statistical analysis

suits best the operational flow of interpolation,
optimization and statistical analysis



Organization of Parallel Computing

organized by Empipe from one of the networked computers (master host)

using standard UNIX protocols (remote shell and equivalent hosts) an EM analysis is started on each of the available hosts

when the analysis is finished on a host, the next job, if any, is dispatched to that host

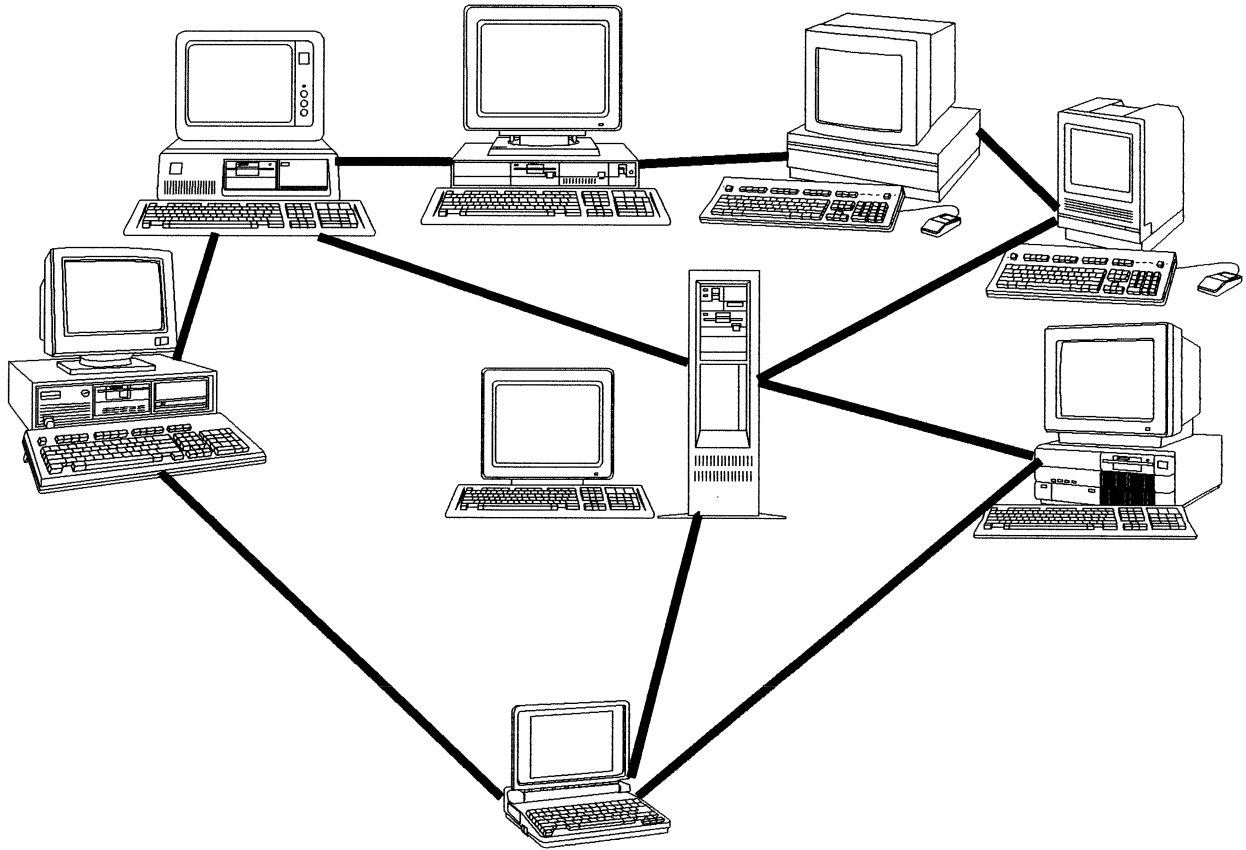
EM simulation results are gathered from all the hosts and stored in a data base created on the master host

no platform specific mechanisms

applicable to both local and wide area networks of heterogeneous workstations



Heterogeneous Network of Computers





Statistical Design of the Attenuator

design specifications (from 2 GHz to 18 GHz)

$$9.5 \text{ dB} \leq \text{insertion loss} \leq 10.5 \text{ dB}$$

$$\text{return loss} \geq 10 \text{ dB}$$

the structure, treated as a whole, is described by 8 geometrical parameters

designable: 4 parameters describing the resistive area

statistical variables: all 8 parameters (with a standard deviation of 0.25 mil)

em simulation at a single frequency requires about 7 CPU minutes on a Sun SPARCstation 1+



Parallel Computing in Nominal Design of the Attenuator

30 *em* analyses

an average of 3.8 analyses run in parallel

about 168 minutes on the network of Sun SPARCstations
1+

time is reduced by 75%

Parallel Computing in Statistical Design of the Attenuator

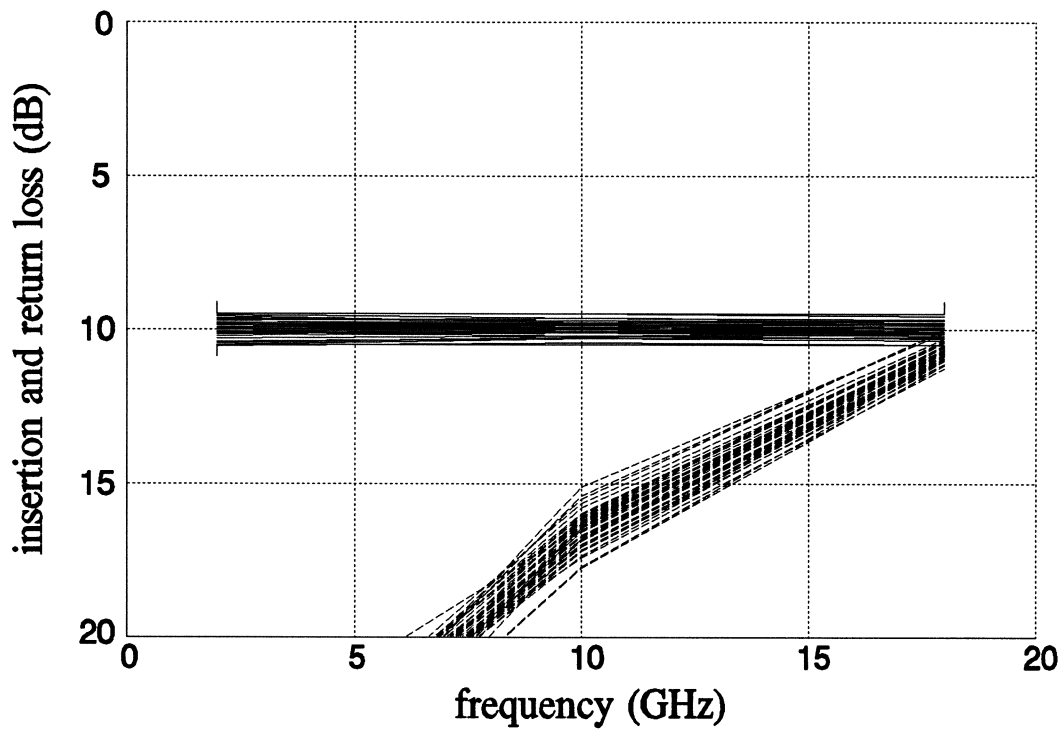
additional 113 *em* analyses

an average of 2.5 analyses run in parallel

time is reduced by 60%



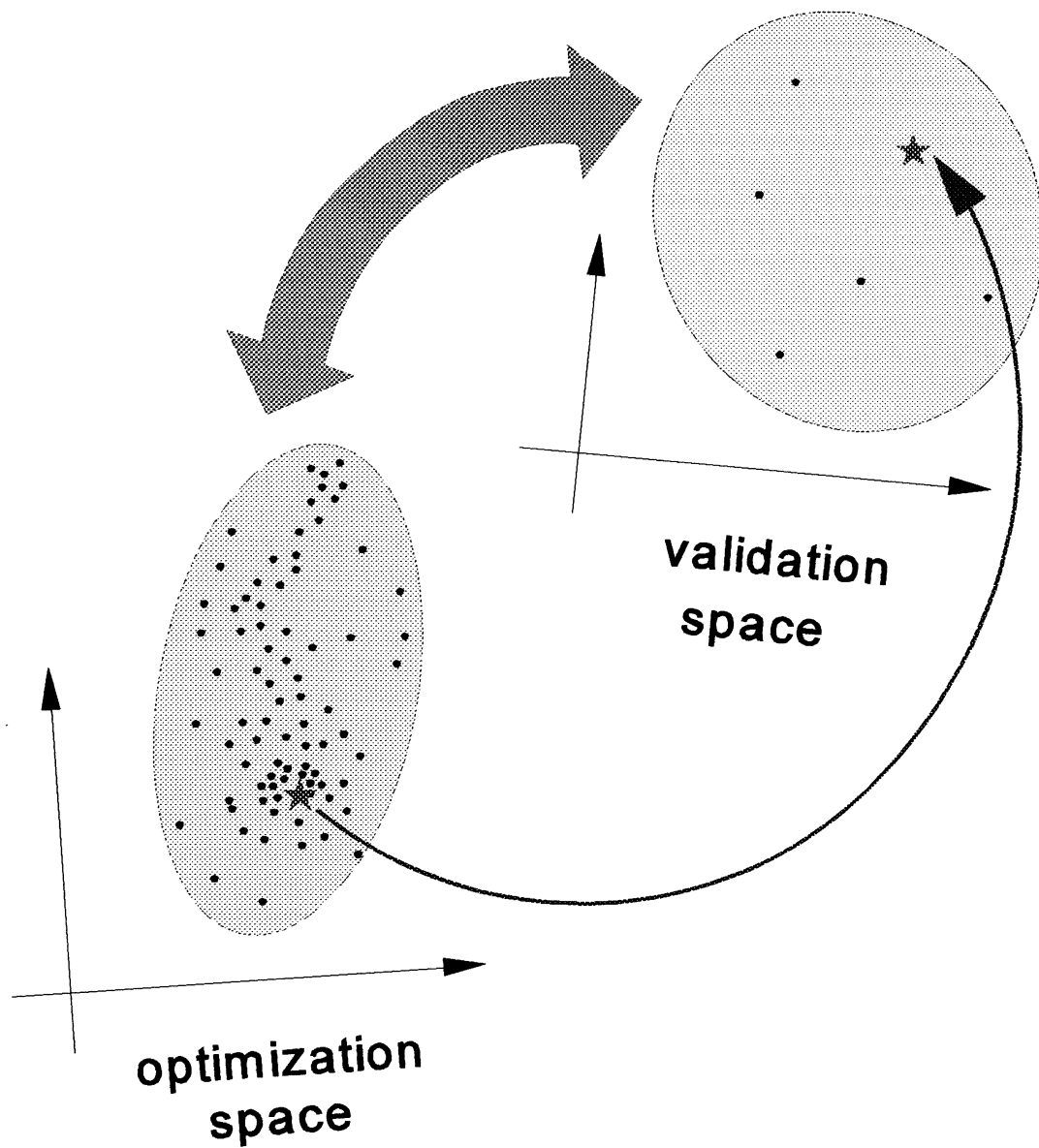
Monte Carlo Sweeps of the Attenuator Responses



yield (estimated from 250 Monte Carlo outcomes) is increased from 82% to 97%



Space Mapping
(Bandler et al., 1994)





Work on Space Mapping

develop theory and corresponding algorithms for parameter space mapping

to allow CPU intensive models to be automatically replaced during optimization by slower but also less accurate models

consider hierarchical family of models: equivalent circuit, empirical, or even decomposed or coarse grid numerical EM models, particularly for arbitrary geometries

aggressive strategy for Space Mapping

automation issues for Space Mapping

expected cornerstone for successful EM optimization

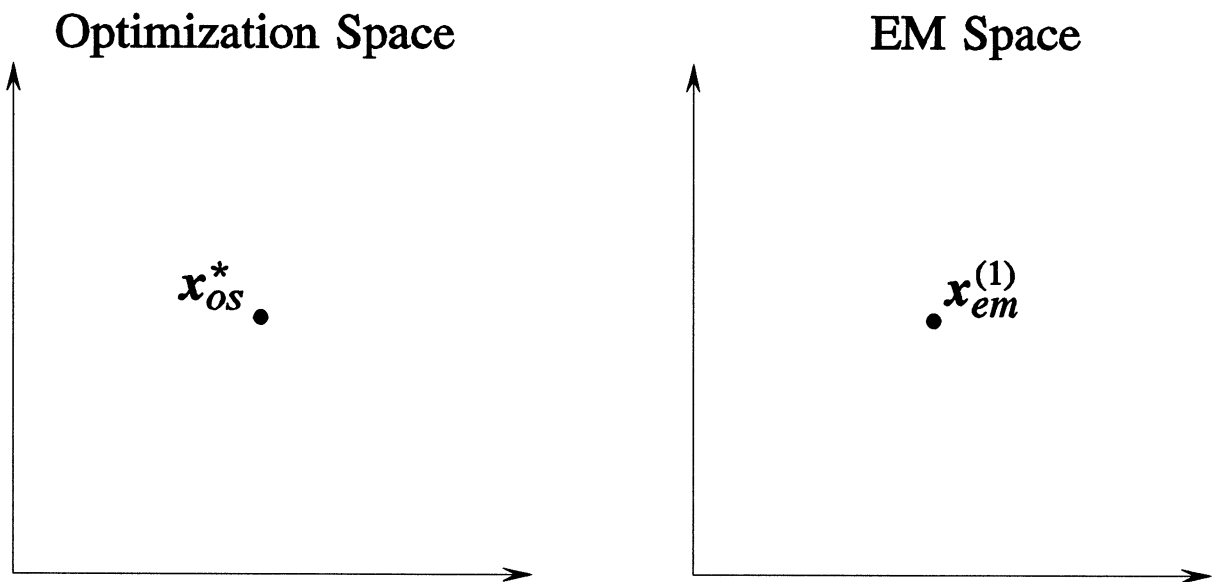


Illustration of Aggressive Space Mapping Optimization

Step 0

find the optimal design x_{os}^* in Optimization Space

Step 1

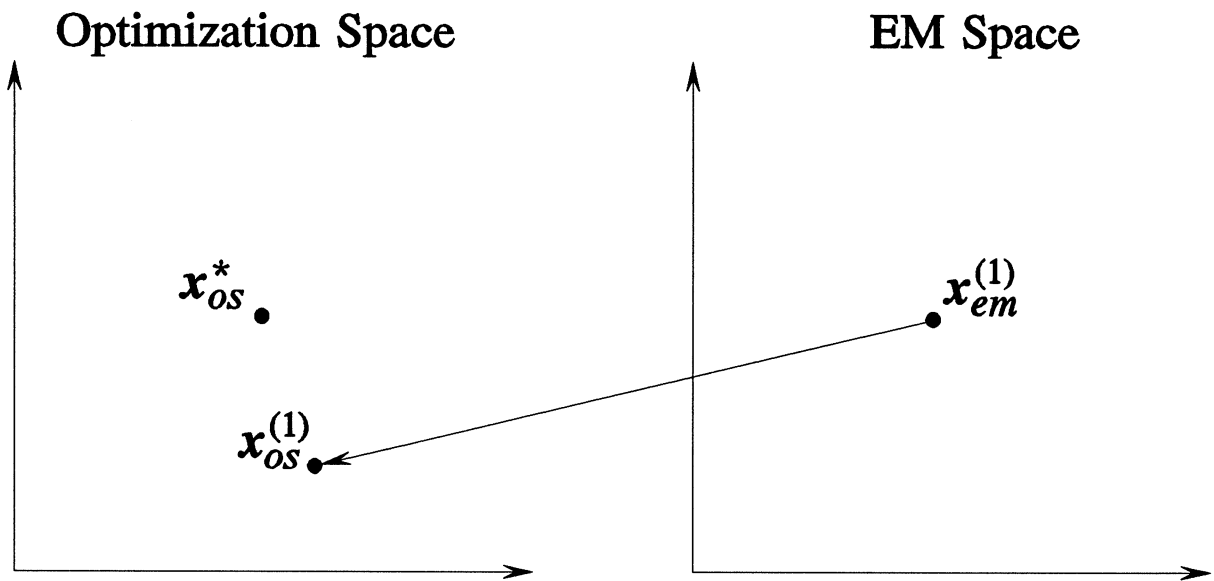


set $x_{em}^{(1)} = x_{os}^*$ assuming x_{em} and x_{os} represent the same physical parameters



Illustration of Aggressive Space Mapping Optimization

Step 2

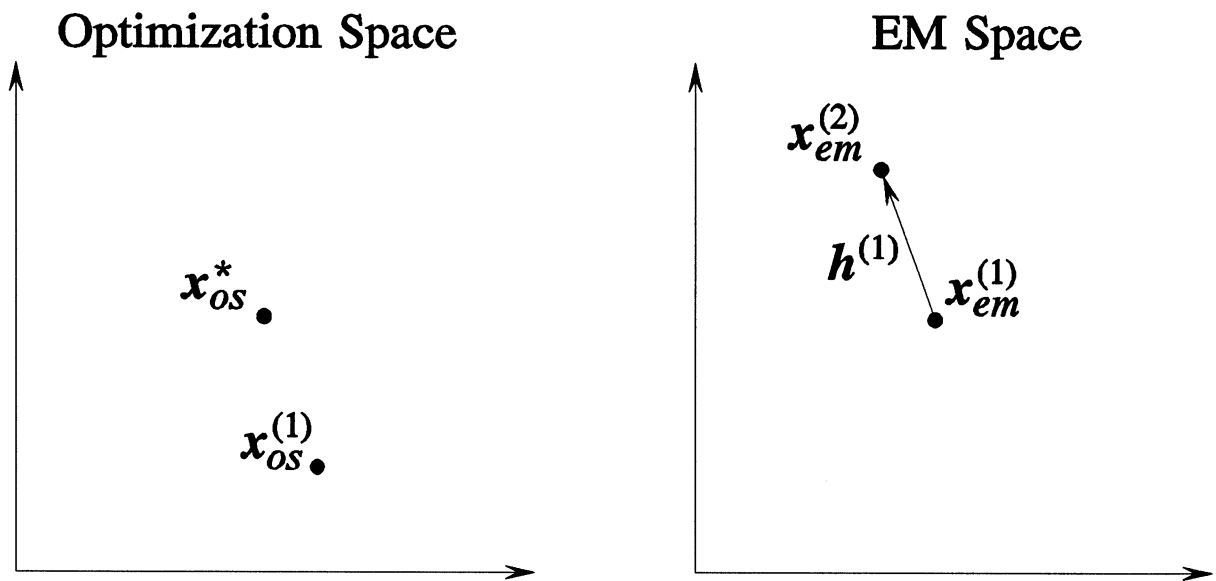


perform X_{os} -space model parameter extraction



Illustration of Aggressive Space Mapping Optimization

Step 3



initialize Jacobian approximation $B^{(1)} = 1$

obtain $x_{em}^{(2)}$ by solving

$$B^{(1)}h^{(1)} = -f^{(1)}$$

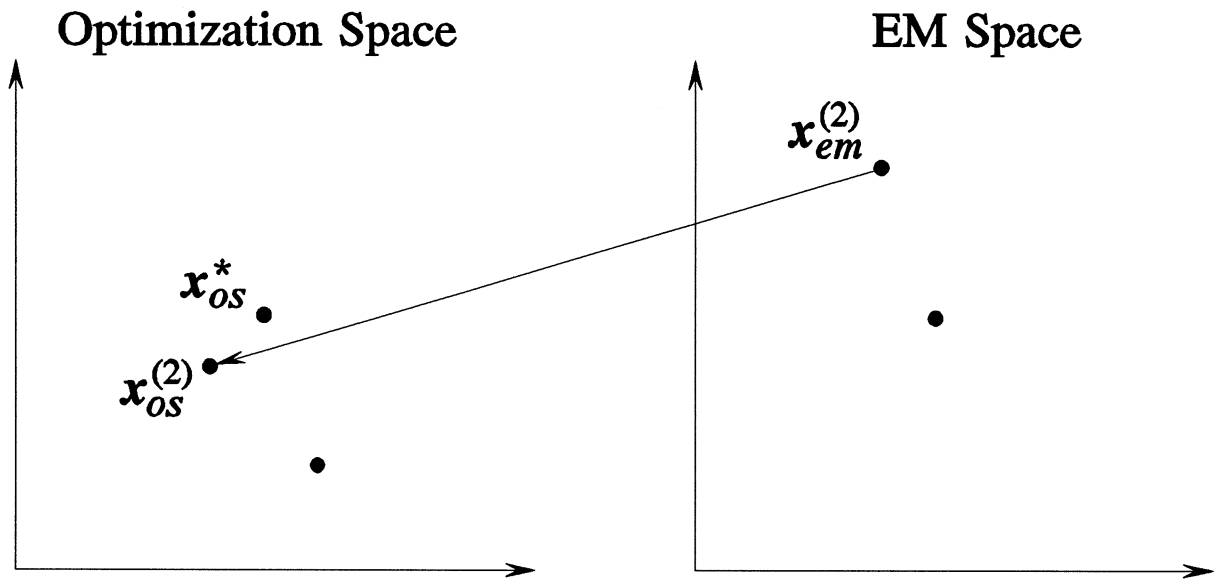
where

$$f^{(1)} = x_{os}^{(1)} - x_{os}^*$$



Illustration of Aggressive Space Mapping Optimization

Step 4

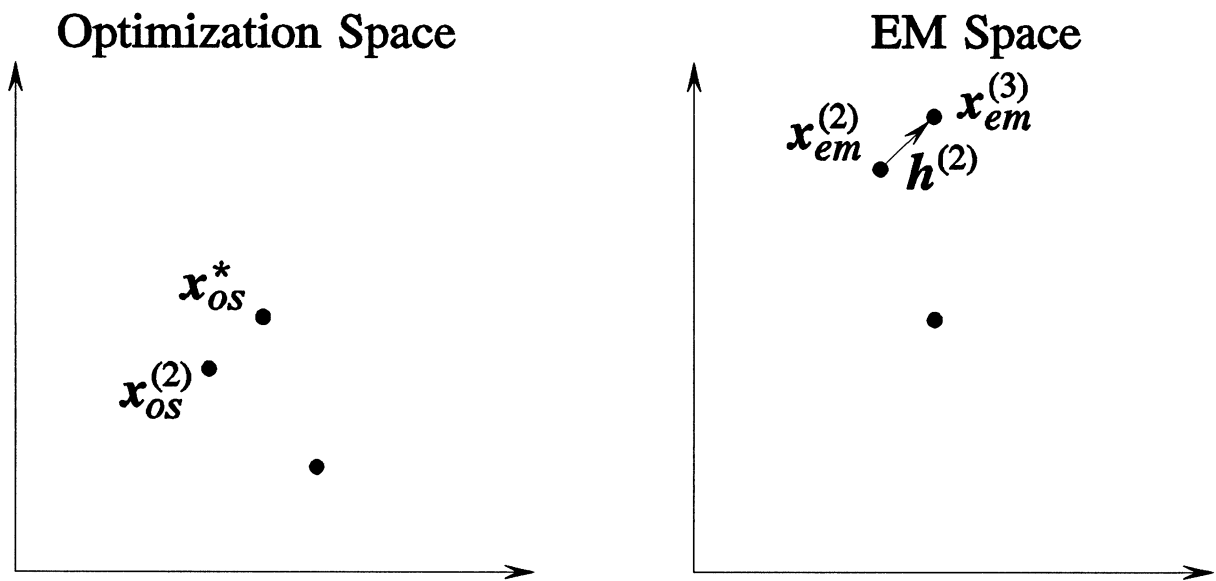


perform X_{os} -space model parameter extraction



Illustration of Aggressive Space Mapping Optimization

Step 5



update Jacobian approximation from $B^{(1)}$ to $B^{(2)}$

obtain $x_{em}^{(3)}$ by solving

$$B^{(2)}h^{(2)} = -f^{(2)}$$

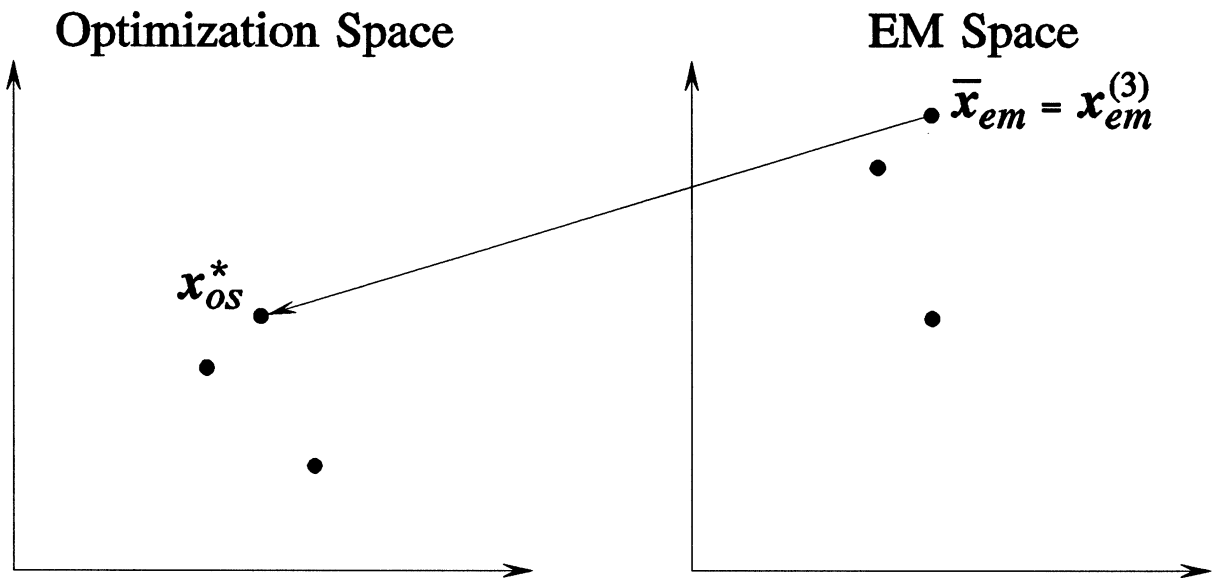
where

$$f^{(2)} = x_{os}^{(2)} - x_{os}^*$$



Illustration of Aggressive Space Mapping Optimization

Step 6



perform X_{os} -space model parameter extraction

if $\|x_{os}^{(3)} - x_{os}^*\| \leq \epsilon$ then $\bar{x}_{em} = x_{em}^{(3)}$ is considered as the SM solution



Automated Aggressive Space Mapping

automating the aggressive SM strategy using a two-level optimization architecture

outer level automates a generic aggressive SM loop including a Broyden update

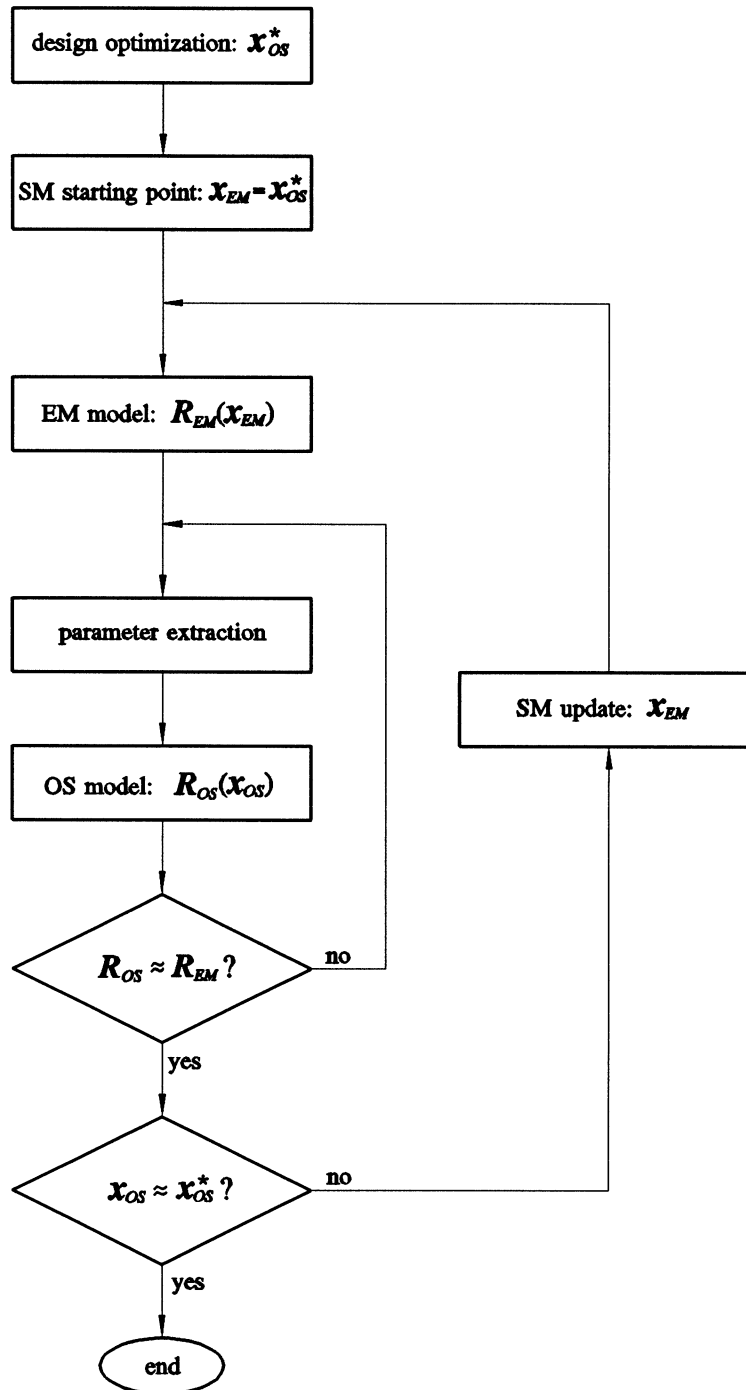
inner level implements parameter extraction for specific models

parameter extraction is crucial to SM optimization

the impact of uniqueness on the convergence of the aggressive SM strategy

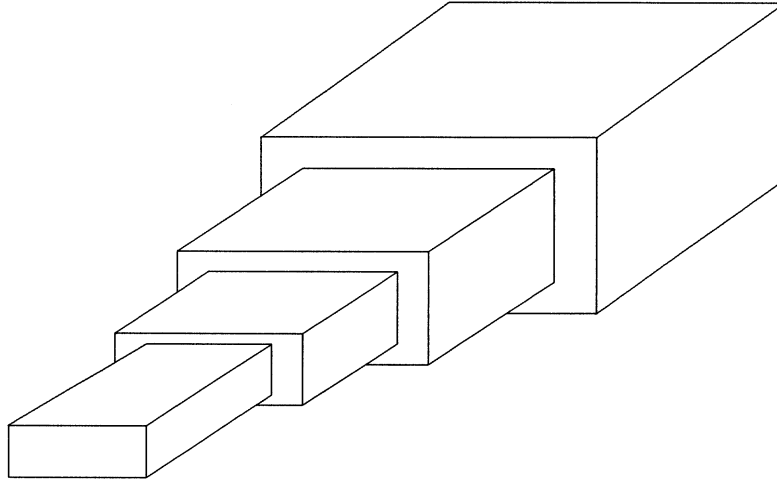


Implementation of Aggressive Space Mapping





Benchmark EM Design Problems EM Optimization of 3D Structures



a two-section waveguide transformer

two cases of Space Mapping used to align

- (a) an ideal empirical model and a non-ideal empirical model
- (b) an empirical model and HFSS simulations



Work in Progress

geometrical decomposition of large systems

as dictated by proximity, EM coupling or higher-order modes and interfaces to various simulators

frequency domain adjoint sensitivities for EM solvers

generalize the adjoint sensitivity analysis technique to general multi-level hierarchical systems

extend our feasible adjoint sensitivity technique (FAST) to handle space-mapped EM sensitivities

investigate how design sensitivity information is transformed/preserved through Space Mapping

yield optimization/design centering

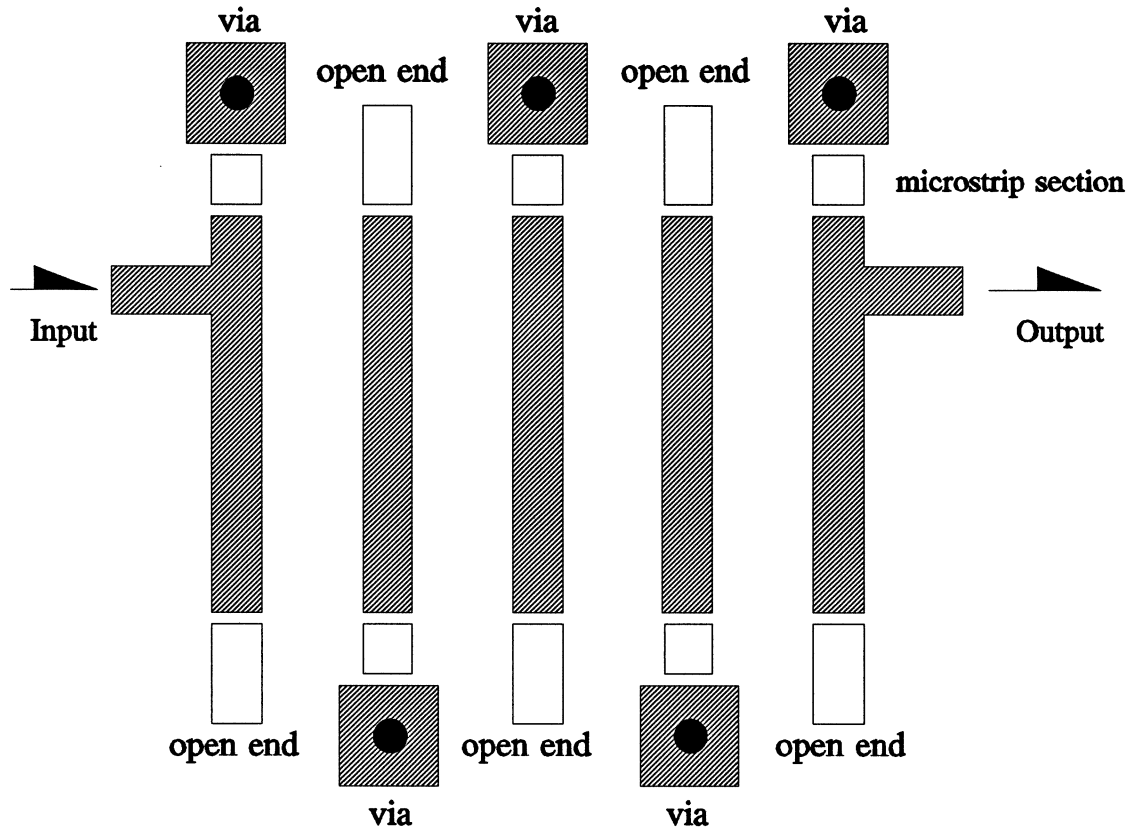
the ultimate benchmark for all algorithms developed within this project

many statistical outcome circuits need to be simulated and checked against design specifications

design visualization and automated documentation



A Coarse Model Using Decomposition



the shadowed areas are calculated by *em* using coarse grid

the other parts are simulated using empirical formulas



Key Interactions

Fritz Arndt

Qian Cai

Shaohua Chen

Marco Dionigi

Craig French

Bill Getsinger

Peter Grobelny

Ron Hemmers

Ya-Fei Huang

Wolfgang Hofer

Nancy Lin

Kaj Madsen

Michel Nahkla

Dzevat Omeragic

Jim Rautio

Poman So

Roberto Sorrentino

Dan Swanson

Salvador Talisa

Quinghui Wang

Qi-Jun Zhang



Conclusions

cost-effective yield-driven design technology is indispensable

EM optimization of arbitrary geometries exerts a massive demand on resources, particularly for yield-driven design

integrated EM simulation and optimization capable of handling arbitrary structures is the future

Space Mapping promises the accuracy of EM simulation and the speed of circuit-level optimization

heterogeneous parallel CAD over a local or wide area network significantly increases design power

user-defined parameterization allows analysis and optimization of complicated structures as a whole

integration of simulators from various sources into automated design optimization with interpolation, response function modeling and data base techniques will immensely reduce the overall design time



Selected References

J.W. Bandler, R.M. Biernacki, S.H. Chen, R.H. Hemmers and K. Madsen, "Electromagnetic optimization exploiting aggressive space mapping," *IEEE Trans. Microwave Theory Tech.*, vol. 43, 1995, pp. 2874-2882.

J.W. Bandler, R.M. Biernacki and S.H. Chen, "Fully automated space mapping optimization of 3D structures," *IEEE MTT-S Int. Microwave Symp.* (San Francisco, CA), June 1996.

J.W. Bandler, R.M. Biernacki and S.H. Chen, "Parameterization of arbitrary geometrical structures for automated electromagnetic optimization," *IEEE MTT-S Int. Microwave Symp.* (San Francisco, CA), June 1996.

J.W. Bandler, R.M. Biernacki, Q. Cai, S.H. Chen and P.A. Grobelny, "Integrated harmonic balance and electromagnetic optimization with Geometry Capture," *IEEE MTT-S Int. Microwave Symp Dig.* (Orlando, FL), 1995, pp. 793-796.

J.W. Bandler, R.M. Biernacki, Q. Cai, S.H. Chen, P.A. Grobelny and D.G. Swanson, Jr., "Heterogeneous parallel yield-driven electromagnetic CAD," *IEEE MTT-S Int. Microwave Symp. Dig.* (Orlando, FL), 1995, pp. 1085-1088.