

## YIELD OPTIMIZATION FOR ARBITRARY STATISTICAL DISTRIBUTIONS

## PART I: THEORY

H.L. Abdel-Malek and J.W. Bandler

Group on Simulation, Optimization and Control  
and Department of Electrical Engineering  
McMaster University, Hamilton, Canada

## ABSTRACT

This paper generalizes certain analytical formulas for yield and yield sensitivities so that design centering and yield optimization can be effectively carried out employing given statistical parameter distributions. The tolerance region of possible outcomes is discretized into a set of orthotopic cells. A suitable weight is assigned to each cell in conjunction with an assumed uniform distribution on the cell. Explicit formulas for yield and its sensitivities are derived. To avoid unnecessary evaluations of circuit responses, multidimensional quadratic interpolation is performed. Sparsity is exploited in the determination of these quadratic models leading to reduced computation as well as increased accuracy.

## INTRODUCTION

The aim of this paper (see also Part II) is to present some theoretical concepts leading to the most general approach currently available for automatic optimization of production yield which avoids the use of the Monte Carlo method. Thus, the design centering and/or optimal tolerance assignment which is to be performed takes explicitly into account statistical distributions and possible parameter correlations.

The approach is based on the work of Bandler, Liu and Tromp [1] and represents a generalization of the work of Bandler and Abdel-Malek [2,3]. The presentation is directed to a nonlinear programming method of solution, and can be associated with original ideas suggested by a number of other researchers [4,5]. Part II of this paper applies this material to the optimization of yield for a current switch emitter follower.

## FUNDAMENTAL CONCEPTS AND DEFINITIONS

A design can be described by a nominal parameter vector  $\phi^0$  of the  $k$  designable parameters

This work was supported by the National Research Council of Canada under Grant A7239.

and a corresponding tolerance vector  $\epsilon$ . The tolerance vector  $\epsilon$  may be used to define the extremes of the tolerance region or the standard deviation, etc. It is assumed that the parameters can be varied continuously.

An outcome  $\{\phi^0, \epsilon, \mu\}$  of a design  $\{\phi^0, \epsilon\}$  implies a point in the parameter space given by

$$\phi = \phi^0 + E \mu, \quad (1)$$

where  $E$  is a diagonal matrix with elements set to  $\epsilon_i$ ,  $i = 1, 2, \dots, k$ , and  $\mu$  is a random vector distributed according to the joint probability distribution function (PDF). The PDF might extend as far as  $(-\infty, \infty)$ , however, for all practical cases it is possible to consider a tolerance region  $R_\epsilon$  such that

$$\int_{R_\epsilon} F(\phi) d\phi_1 d\phi_2 \dots d\phi_k = 1, \quad (2)$$

where  $F(\phi)$  is the PDF.

For the sake of simplicity as well as the implications of independent design parameters, there is no loss of generality to consider  $R_\epsilon$  to be an orthotope defined by

$$R_\epsilon \triangleq \{\phi \mid \phi = \phi^0 + E \mu, \mu \in R_\mu\}, \quad (3)$$

where

$$R_\mu \triangleq \{\mu \mid -1 \leq \mu_i \leq 1, i = 1, 2, \dots, k\}. \quad (4)$$

This orthotope is centered at  $\phi^0$  and has edges of length  $2\epsilon_i$ ,  $i = 1, 2, \dots, k$ . The extreme points of  $R_\epsilon$  are called vertices and the set of vertices is defined by [1]

$$R_v \triangleq \{\phi \mid \phi_i = \phi_i^0 + \epsilon_i \mu_i, \mu_i \in \{-1, 1\}, i = 1, 2, \dots, k\}. \quad (5)$$

The number of these vertices is  $2^k$  and for

$$\phi^r = \phi^0 + E \mu^r, \mu_i^r \in \{-1, 1\} \quad (6)$$

we have

$$r = 1 + \sum_{i=1}^k \left(\frac{\mu_i^r + 1}{2}\right) 2^{i-1}. \quad (7)$$

The constraint region (or feasible region)



$$h_{ij} = h_{ji} = [g(\underline{\phi}^l) - g(\underline{\phi}^N) - (\zeta_i^j)^2 \frac{h_{ii}}{2} - (\zeta_j^i)^2 \frac{h_{jj}}{2} - \zeta_i^j a_i - \zeta_j^i a_j] / \zeta_i^j \zeta_j^i, \quad (29)$$

where

$$l = j - i + \sum_{p=1}^i (k - p + 1), \quad j > i \quad (30)$$

and

$$\zeta_i^j = u_{j-i, k-i} \delta_i, \quad \zeta_j^i = T_{j-i, k-i} \delta_j, \quad i < j. \quad (31)$$

Subsequently, the number of multiplications/divisions required to obtain the approximation is

reduced to  $5k^2 - 2k$  instead of  $(N^3 + 3N^2 - N)/3$  for Gauss elimination, where  $N$  is defined in (10).

Fig. 1 shows the choice of base points in two dimensions and three dimensions [2].

If we are not completely free in choosing the base points, for example, if the function evaluation is expensive and some evaluations,  $n$  say, for parameter values inside the interpolation region are known, the linear equations can be ordered such that these  $n$  equations come last. In solving the resulting system of simultaneous equations, we proceed with finding the polynomial coefficients using (27), (28) and (29) until we come to the full part of the matrix, i.e., the last  $n$  equations. The unknown coefficients beyond this point should be found by solving  $n$  simultaneous linear equations, for example, by Gauss elimination.

#### EVALUATION OF YIELD AND ITS SENSITIVITIES

##### The Linear Cut [2]

In order to obtain the linear cuts required for yield evaluation [2], consider linearizing the quadratic constraints at a point  $\underline{\phi}^a$  which may, for example, be the nominal point  $\underline{\phi}^0$  or a vertex  $\underline{\phi}^r$ . Hence, the linear cut based upon the  $l$ th constraint is given by

$$g_l(\underline{\phi}^a) + (\underline{\phi} - \underline{\phi}^a)^T \underline{v}_l g_l(\underline{\phi}^a) \geq 0. \quad (32)$$

Define a reference vertex  $\underline{\phi}^r$  by

$$\underline{\phi}^r = \underline{\phi}^0 + \underline{E} \underline{\mu}^r, \quad (33)$$

where

$$\mu_j^r = -\text{sign} \left( \frac{\partial g_l(\underline{\phi}^a)}{\partial \phi_j} \right), \quad j = 1, 2, \dots, k. \quad (34)$$

The distance from the reference vertex to the point of intersection with the  $l$ th cut along the orthotope edge in the  $j$ th direction is

$$\alpha_j^l = \mu_j^r [g_l(\underline{\phi}^a) + (\underline{\phi}^r - \underline{\phi}^a)^T \underline{v}_l g_l(\underline{\phi}^a)] / \left( \frac{\partial g_l(\underline{\phi}^a)}{\partial \phi_j} \right). \quad (35)$$

Accordingly, we have

$$\begin{aligned} \frac{\partial \alpha_j^l}{\partial \phi_j^0} &= \mu_j^r \left[ \frac{\partial g_l(\underline{\phi}^a)}{\partial \phi_j} + (\underline{\phi}^r - \underline{\phi}^a)^T \underline{H}_l \right] / \left( \frac{\partial g_l(\underline{\phi}^a)}{\partial \phi_j} \right) \\ &- \mu_j^r \left[ g_l(\underline{\phi}^a) + (\underline{\phi}^r - \underline{\phi}^a)^T \underline{v}_l g_l(\underline{\phi}^a) \right] H_{ji} / \left( \frac{\partial g_l(\underline{\phi}^a)}{\partial \phi_j} \right)^2, \end{aligned} \quad (36)$$

is the Hessian matrix which is a constant matrix for a quadratic function  $g_l(\underline{\phi})$ ,  $H_{ji}$  is the  $i$ th column of  $H$  and  $H_{ji}$  is an element of  $H$ . In deriving (36) it is assumed that  $(\underline{\phi}^r - \underline{\phi}^a)$  is independent of  $\phi_i$ ,  $i = 1, 2, \dots, k$ .

##### The General Distribution

As described earlier, we can assume that all outcomes will lie within the tolerance orthotope  $R$ . This orthotope is now partitioned into a set of orthocells  $R(i_1, i_2, \dots, i_k)$  as shown in Fig. 2, where  $i_j = 1, 2, \dots, n_j$ ,  $n_j$  is the number of intervals in the  $j$ th direction and  $j = 1, 2, \dots, k$ . A weighting factor  $W(i_1, i_2, \dots, i_k)$  is assigned to each orthocell and is given by

$$W(\underline{i}) = w(\underline{i}) / V(R(\underline{i})), \quad (37)$$

where

$$\underline{i} = (i_1, i_2, \dots, i_k), \quad (38)$$

$$w(\underline{i}) = \int_{R(\underline{i})} F(\underline{\phi}) dv, \quad (39)$$

$$V(R(\underline{i})) = \int_{R(\underline{i})} dv = \prod_{j=1}^k \epsilon_{j, i_j}, \quad (40)$$

$$dv = d\phi_1 d\phi_2 \dots d\phi_k, \quad (41)$$

$\epsilon_{1, i_1}, \epsilon_{2, i_2}, \dots, \epsilon_{k, i_k}$  are the dimensions of the orthocell and  $F(\underline{\phi})$  is the joint probability distribution function (PDF).

The weighting factors  $W(\underline{i})$  can also be obtained by sampling the parameters or from a histogram if the PDF is not available.

In principle, the problem of finding the yield is now reduced to finding the contribution to the yield given by all of these orthocells. A formula for the weighted nonfeasible hypervolume with respect to the  $l$ th constraint is constructed and is given by [3]

$$V^l = \left( \frac{1}{k!} \prod_{j=1}^k \alpha_j^l \right) \left[ \begin{array}{ccc} n_1+1 & n_2+1 & n_k+1 \\ \Sigma & \Sigma & \dots & \Sigma & \Delta W(\underline{i}) (\delta^l(\underline{i}))^k \\ i_1=1 & i_2=1 & & i_k=1 \end{array} \right], \quad (42)$$

where, for indexing with respect to  $\underline{\phi}^r$ , i.e., numbering starts at this vertex (see Fig. 2),  $\alpha_j^l$  is the distance from the reference vertex to the point of intersection of the  $l$ th linear cut with the orthotope edge in the  $j$ th direction,

$$\delta^l(\underline{i}) = \max \left( 0, 1 - \sum_{j=1}^k \frac{1}{\alpha_j^l} \sum_{p=1}^{i_j} \epsilon_{j,p-1} \right), \quad (43)$$

$$\epsilon_{j,0} = 0, \quad j = 1, 2, \dots, k, \quad (44)$$

$$\begin{aligned} \Delta W(\underline{i}) = & W(\underline{i}) - \sum_{j=1}^k W(\underline{i} - \underline{e}_j) + \sum_{j=1}^{k-1} \sum_{p=j+1}^k W(\underline{i} - \underline{e}_j - \underline{e}_p) - \dots \\ & + (-1)^k W(\underline{i} - \underline{e}_1 - \underline{e}_2 - \dots - \underline{e}_k), \quad (45) \end{aligned}$$

$$\underline{e}_j = (0, 0, \dots, 0, \underset{j}{1}, 0, \dots, 0) \quad (46)$$

and where

$$W(\underline{i}) = 0 \text{ if } i_j = 0 \text{ or } i_j = n_j + 1 \text{ for any } j. \quad (47)$$

Assuming no overlapping of nonfeasible regions defined by different cuts inside the orthotope  $R_\epsilon$ , i.e.,

$$R_i \cap R_j = \emptyset, \quad i \neq j, \quad (48)$$

where

$$R_\ell = \{ \phi \mid g_\ell(\phi) < 0 \} \cap R_\epsilon, \quad (49)$$

the yield can be expressed as

$$Y = 1 - \sum_{\ell=1}^m V^\ell, \quad (50)$$

where  $m$  is the number of linear cuts.

### Independent Parameters

In the case of independent parameters, (42) can be written as [3]

$$V^\ell = \left( \frac{1}{k!} \prod_{j=1}^k \alpha_j^l \right) \left[ \begin{array}{ccc} \sum_{i_1=1}^{n_1+1} \Delta W_1(i_1) & \sum_{i_2=1}^{n_2+1} \Delta W_2(i_2) & \dots \\ \sum_{i_k=1}^{n_k+1} \Delta W_k(i_k) (\delta^l(\underline{i}))^k & & \end{array} \right], \quad (51)$$

where  $\underline{i}$  and  $\delta^l(\underline{i})$  are as defined in (38) and (43), respectively, and where

$$\Delta W_j(i_j) = W_j(i_j) - W_j(i_j - 1), \quad j = 1, 2, \dots, k, \quad (52)$$

$$W_j(0) = W_j(n_j + 1) = 0, \quad j = 1, 2, \dots, k, \quad (53)$$

$$W_j(i_j) = w_j(i_j) / \epsilon_{j,i_j}, \quad i_j = 1, 2, \dots, n_j, \quad (54)$$

$$w_j(i_j) = \int_{R_j(i_j)} f_j(\phi_j) d\phi_j, \quad i_j = 1, 2, \dots, n_j, \quad (55)$$

$f_j(\phi)$  is the PDF of the  $j$ th parameter and  $R_j(i_j)$  is the  $i$ th interval for that parameter. Similarly the yield will be given by (50).

### Yield Sensitivities

Formulas for yield sensitivities can be derived assuming that the weighting factors  $W(\underline{i})$  are independent of  $\phi_j^0$  as long as the ratios between  $\epsilon_{j,i_j}$ ,  $i_j = 1, 2, \dots, n_j$ , are fixed for each parameter  $j = 1, 2, \dots, k$ . This is true, for example, if the sizes of the orthocells are fixed.

Let

$$\kappa_{j,i_j} = \epsilon_{j,i_j} / \epsilon_j, \quad (56)$$

hence,

$$\sum_{i_j=1}^{n_j} \kappa_{j,i_j} = 2, \quad j = 1, 2, \dots, k. \quad (57)$$

The yield sensitivities are now given by

$$\frac{\partial Y}{\partial \phi_i^0} = - \sum_{\ell=1}^m \frac{\partial V^\ell}{\partial \phi_i^0}, \quad (58)$$

$$\frac{\partial Y}{\partial \epsilon_i} = - \sum_{\ell=1}^m \frac{\partial V^\ell}{\partial \epsilon_i}, \quad (59)$$

where

$$\begin{aligned} \frac{\partial V^\ell}{\partial \phi_i^0} = & \left( \frac{1}{k!} \sum_{j=1}^k \frac{\partial \alpha_j^l}{\partial \phi_i^0} \prod_{p=1}^k \alpha_p^l \right) B + A \left[ \begin{array}{ccc} \sum_{i_1=1}^{n_1+1} \Delta W_1(i_1) & \sum_{i_2=1}^{n_2+1} \Delta W_2(i_2) & \dots \\ \sum_{i_k=1}^{n_k+1} \Delta W_k(i_k) (\delta^l(\underline{i}))^k & & \end{array} \right] \frac{\partial \delta^l(\underline{i})}{\partial \phi_i^0}, \quad (60) \end{aligned}$$

$$\frac{\partial V^\ell}{\partial \epsilon_i} = \left( \frac{\mu_i^r}{k!} \sum_{j=1}^k \frac{\partial \alpha_j^l}{\partial \epsilon_i} \prod_{p=1}^k \alpha_p^l \right) B + A \left[ \begin{array}{ccc} \sum_{i_1=1}^{n_1+1} \Delta W_1(i_1) & \sum_{i_2=1}^{n_2+1} \Delta W_2(i_2) & \dots \\ \sum_{i_k=1}^{n_k+1} \Delta W_k(i_k) (\delta^l(\underline{i}))^k & & \end{array} \right] \frac{\partial \delta^l(\underline{i})}{\partial \epsilon_i}, \quad (61)$$

$$A = \frac{1}{k!} \prod_{j=1}^k \alpha_j^l, \quad (62)$$

$$B = \sum_{i_1=1}^{n_1+1} \sum_{i_2=1}^{n_2+1} \dots \sum_{i_k=1}^{n_k+1} \Delta W(\underline{i}) (\delta^l(\underline{i}))^k \quad (63)$$

and where

$$\frac{\partial \delta^l(\underline{i})}{\partial \phi_i^0} = \begin{cases} 0 & \text{if } \delta^l(\underline{i}) = 0, \\ \frac{k}{\sum_{j=1}^k \frac{1}{(\alpha_j^l)^2} \frac{\partial \alpha_j^l}{\partial \phi_i^0} \sum_{p=1}^{i_j} \epsilon_{j,p-1}} & \text{if } \delta^l(\underline{i}) > 0, \end{cases} \quad (64)$$

$$\frac{\partial \delta^l(\underline{i})}{\partial \epsilon_i} = \mu_i^r \frac{\partial \delta^l(\underline{i})}{\partial \phi_i^0} - \sum_{j=1}^k \frac{1}{\alpha_j^l} \sum_{p=1}^{i_j} \kappa_{j,p-1}. \quad (65)$$

The formulas for  $\partial \alpha_j^l / \partial \phi_i^0$  and for  $\mu_i^r$  are given by (36) and (34), respectively.

The case of independent parameters is obtained by substituting

$$\Delta W(i_j) = \prod_{j=1}^k \Delta W_j(i_j) \quad (66)$$

in (60), (61) and (63).

#### Example

In order to illustrate the calculation of the weighted hypervolume, consider the two-dimensional example shown in Table I. The reference vertex  $\phi^r$  is given by  $\mu_1^r = -1$ ,  $\mu_2^r = 1$  while  $\alpha_1 = 12$  and  $\alpha_2 = 3$ . The weighted volume is given by

$$V = \left( \frac{1}{2} \times 12 \times 3 \right) \sum_{i_1=1}^4 \sum_{i_2=1}^3 \Delta W(i_1, i_2) (\delta(i_1, i_2))^2 \\ = 1813/3600 .$$

The same example can be considered as if the parameters are independent as shown in Table II and Table III. The same weighted volume will obviously be obtained.

Assuming that the sizes of the orthocells are fixed, the sensitivities of the weighted hypervolume with respect to the nominal parameter vector  $\phi^0$  can be evaluated. The location of  $\phi^0$  itself is not important. It is the relative location of the constraint with respect to the orthotope that matters. The constraint can be considered as

$$\phi_1/12 - \phi_2/3 \geq 0 .$$

According to (36) we have

$$\partial \alpha_1 / \partial \phi_1^0 = -1, \quad \partial \alpha_1 / \partial \phi_2^0 = 4, \quad \partial \alpha_2 / \partial \phi_1^0 = -1/4$$

$$\text{and } \partial \alpha_2 / \partial \phi_2^0 = 1 .$$

Using (64), the values of  $\partial \delta^k(i_j) / \partial \phi_1^0$  are given in Table IV and Table V. Substituting in (60) we get

$$\frac{\partial V}{\partial \phi_1^0} = -43/720, \quad \frac{\partial V}{\partial \phi_2^0} = 43/180 .$$

These sensitivities were verified numerically.

#### CONCLUSIONS

The yield estimation technique presented provides an inexpensive yield determination without the need for the multitude of circuit simulations required in the Monte Carlo method. The method approximates the integration of the PDF over the feasible region. In addition, the availability of yield sensitivities permits the use of efficient gradient optimization techniques (see Part II). The exploitation of sparsity in choosing the base points reduces the computational effort required for interpolation significantly. A full description of this work is available [7].

#### REFERENCES

- [1] J.W. Bandler, P.C. Liu and H. Tromp, "A nonlinear programming approach to optimal design centering, tolerancing and tuning", IEEE Trans. Circuits and Systems, vol. CAS-23, March 1976, pp. 155-165.
- [2] J.W. Bandler and H.L. Abdel-Malek, "Optimal centering, tolerancing and yield determination using multidimensional approximations", Proc. 1977 IEEE Symp. on Circuits and Systems (Phoenix, AZ, April 1977), pp. 219-222.
- [3] H.L. Abdel-Malek and J.W. Bandler, "Yield estimation for efficient design centering assuming arbitrary statistical distributions", Int. J. Circuit Theory and Applications, to appear.
- [4] B.J. Karafin, "The general component tolerance assignment problem in electrical networks", Ph.D. Thesis, Univ. of Pennsylvania, Philadelphia, PA, 1974.
- [5] T.R. Scott and T.P. Walker, "Regionalization: a method for generating joint density estimates", IEEE Trans. Circuits and Systems, vol. CAS-23, April 1976, pp. 575-578.
- [6] H.C. Thacher, Jr., and W.E. Milne, "Interpolation in several variables", SIAM J., vol. 6, 1960, pp. 33-42.
- [7] H.L. Abdel-Malek and J.W. Bandler, "Yield optimization for arbitrary statistical distributions, Part I: Theory", Faculty of Engineering, McMaster University, Hamilton, Canada, Report SOC-184, 1977.

TABLE I  
EXAMPLE OF GENERAL HYPERVOLUME CALCULATION

Orthocell	$i_1$	0	1	2	3	4	
dimensions	$\epsilon_{1,i_1}$	0	3.0	3.0	2.0	-	
	$i_2$	$\epsilon_{2,i_2}$					
0	0	w,W	0	0	0	0	
		w	0	18/100	12/100	3/10	0
1	2.0	W	0	3/100	1/50	3/40	0
		$\Delta W$	-	3/100	-1/100	11/200	-3/40
		$\delta$	-	1	3/4	1/2	1/3
2	3.0	w	0	12/100	8/100	2/10	0
		W	0	1/75	2/225	1/30	0
		$\Delta W$	-	-1/60	1/180	-11/360	1/24
		$\delta$	-	1/3	1/12	0	0
3	-	w,W	0	0	0	0	0
		$\Delta W$	-	-1/75	1/225	-11/450	1/30
		$\delta$	-	0	0	0	0

TABLE II  
LENGTHS AND WEIGHTS OF FIRST PARAMETER INTERVALS

$i_1$	$\epsilon_{1,i_1}$	$w(i_1)$	$W(i_1)$	$\Delta W(i_1)$
0	0.0	0	0	-
1	3.0	3/10	1/10	1/10
2	3.0	2/10	1/15	-1/30
3	2.0	5/10	1/4	11/60
4	-	0	0	-1/4

TABLE III  
LENGTHS AND WEIGHTS OF SECOND PARAMETER INTERVALS

$i_2$	$\epsilon_{2,i_2}$	$w(i_2)$	$W(i_2)$	$\Delta W(i_2)$
0	0.0	0	0	-
1	2.0	6/10	3/10	3/10
2	3.0	4/10	2/15	-1/6
3	-	0	0	-2/15

TABLE IV  
VALUES OF  $\partial \delta^k(i_1, i_2) / \partial \phi_1^0$

$i_2 \setminus i_1$	1	2	3	4
1	0	-1/48	-1/24	-1/18
2	-1/18	-11/144	0	0
3	0	0	0	0

TABLE V  
VALUES OF  $\partial \delta^k(i_1, i_2) / \partial \phi_2^0$

$i_2 \setminus i_1$	1	2	3	4
1	0	1/12	1/6	2/9
2	2/9	11/36	0	0
3	0	0	0	0

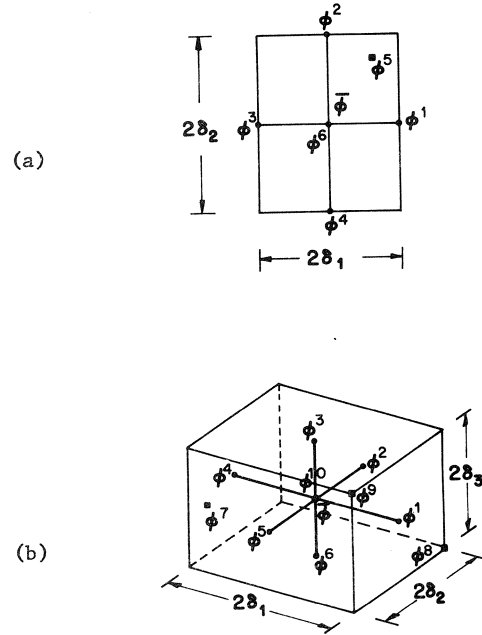


Fig. 1 Arrangement of the base points w.r.t. the centers of interpolation regions (a) two dimensions and (b) three dimensions. For the sparse formulation  $\phi^7$ ,  $\phi^8$  and  $\phi^9$  are, respectively, placed in the planes containing  $\{\bar{\phi}, \phi^1, \phi^2\}$ ,  $\{\bar{\phi}, \phi^1, \phi^3\}$  and  $\{\bar{\phi}, \phi^2, \phi^3\}$ .

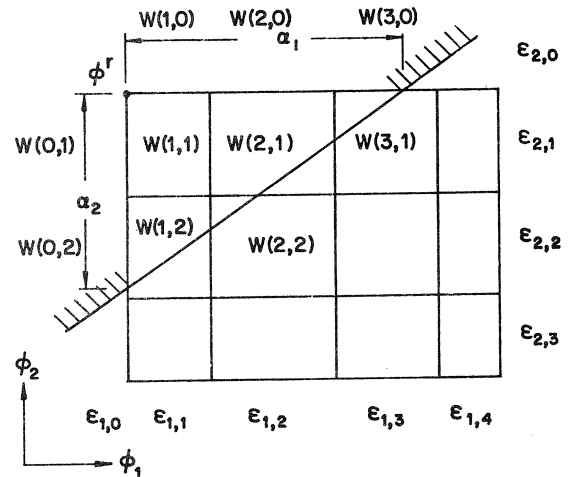


Fig. 2 Two-dimensional illustration of the partitioning of the tolerance region into cells indicating the dimensions and weighting of those cells relevant to the calculation of the weighted nonfeasible hypervolume.