Space Mapping With Multiple Coarse Models for Optimization of Microwave Components

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Abstract—The performance of space mapping (SM) optimization algorithms depends primarily on the quality of the underlying coarse model. Models available in the microwave area can be cheap but inaccurate or accurate but too expensive. Here, we consider a multicoarse-model technique that allows us to combine the merits of both types of coarse models to substantially reduce the overall computational cost of optimization in comparison to traditional SM.

Index Terms—Coarse model, engineering optimization, microwave design, space mapping (SM) optimization.

I. INTRODUCTION

T is well known [1], [2] that the performance of a space mapping (SM) optimization algorithm depends on the quality of the underlying coarse model, which should be as good a representation of the fine model to be optimized as possible but also significantly less expensive than the fine model. Under these conditions, an SM algorithm can reach a satisfactory solution after a few fine model evaluations.

Available coarse models are either cheap but inaccurate, e.g., an equivalent circuit, or accurate but too expensive, e.g., a microwave structure evaluated using the same simulator as the fine model but with a coarser mesh. In the first case, the SM optimization process exhibits computational overhead due to the excessive fine model evaluations necessary to find a good solution or the SM algorithm fails to find a satisfactory solution. In the latter case, the cost of solving the parameter extraction and surrogate optimization sub-problems, normally negligible, may determine the cost of SM optimization.

A multimodel aggressive SM [3] deals with these problems through fine models of increasing accuracy. The outcome of the optimization stage using the less accurate model is the starting point for the next stage using the more accurate model. This increases the chance for SM to find a good solution although the optimization time savings are limited.

The concept of a dynamic coarse model combining the equivalent-circuit and coarse electromagnetic (EM) model and ap-

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plied to SM optimization of LTCC radio frequency (RF) circuits was presented in [4].

An interpolation technique described in [5] allows us to create coarse models that are both accurate and sufficiently cheap. The coarse model (accurate but too expensive to be directly employed in the SM algorithm) is evaluated on a relatively coarse simulation grid and the modified model is obtained by interpolating this data. Hence, the coarse model is evaluated at a limited number of points which allows us to reduce the SM optimization time. This technique is efficient if the number of design variables n is small (i.e., n < 5) [5].

Here we propose a multiple-coarse-model SM technique in which the accuracy of the basic coarse model is enhanced through standard SM modeling using the auxiliary coarse model (more accurate but too expensive to be directly used in SM optimization; typically, it is the model utilizing the same EM simulator as the fine model but with a coarser mesh). Our technique retains all the advantages of the method [5] but is not limited to a small number of design variables.

II. MULTICOARSE-MODEL SPACE MAPPING OPTIMIZATION

Let R_f denote the response vector of a fine model of the device of interest. Our goal is to solve

$$\boldsymbol{x}_{f}^{*} = \arg\min_{\boldsymbol{x}} U(\boldsymbol{R}_{f}(\boldsymbol{x})) \tag{1}$$

where U is a given objective function. We consider an optimization algorithm that generates a sequence of points $\boldsymbol{x}^{(i)}, i = 0, 1, 2, \ldots$, and a family of surrogate models $\boldsymbol{R}^{(i)}_s$, so that

$$\boldsymbol{x}^{(i+1)} = \arg\min_{\boldsymbol{x}} U(\boldsymbol{R}_s^{(i)}(\boldsymbol{x})).$$
(2)

Let \mathbf{R}_c denote the response vector of the coarse model: less accurate than the fine model but much faster to evaluate. Standard SM [1], [2] assumes that models $\mathbf{R}_s^{(i)}$ are constructed from the coarse model so that the misalignment between $\mathbf{R}_s^{(i)}$ and the fine model is minimized. Let $\mathbf{\bar{R}}_s$ be a generic SM surrogate model, i.e., the coarse model composed with suitable SM transformations. The surrogate model $\mathbf{R}_s^{(i)}$ is defined as

$$\boldsymbol{R}_{s}^{(i)}(\boldsymbol{x}) = \bar{\boldsymbol{R}}_{s}(\boldsymbol{x}, \boldsymbol{p}^{(i)}) \tag{3}$$

where

$$\boldsymbol{p}^{(i)} = \arg\min_{\boldsymbol{p}} \sum_{k=0}^{i} w_{i,k} ||\boldsymbol{R}_f(\boldsymbol{x}^{(k)}) - \bar{\boldsymbol{R}}_s(\boldsymbol{x}^{(k)}, \boldsymbol{p})|| \quad (4)$$

is a vector of model parameters and $w_{i,k}$ are weighting factors.

A variety of SM models is available [1], [2], e.g., the input SM [1], where \bar{R}_s takes the form $\bar{R}_s(x, p) = \bar{R}_s(x, B, c) = R_c(B \cdot x + c)$. Typically, the starting point $x^{(0)}$ of the SM algorithm is a coarse model optimum, i.e., $x^{(0)} = \arg \min\{x : U(R_c(x))\}$.

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Fig. 1. Third-order Chebyshev bandpass filter [7].

We propose here a multicoarse-model SM algorithm which assumes the two coarse models: R_{c1} —very cheap to evaluate but not necessarily accurate, and R_{c2} -expensive but much more accurate than R_{c1} . R_{c1} could be a circuit equivalent of the microwave structure, R_{c2} could be a model implemented with the same EM simulator as the fine model but using a coarser mesh. We require that a few evaluations of R_{c2} take less time than a single evaluation of R_f .

We enhance R_{c1} using $\dot{R_{c2}}$ and a standard SM modeling methodology [1], [2]. We define an enhanced coarse model as

$$\boldsymbol{R}_{c}(\boldsymbol{x}) = \boldsymbol{A} \cdot \boldsymbol{R}_{c1}(\boldsymbol{B} \cdot \boldsymbol{x} + \boldsymbol{c}) \tag{5}$$

with parameters A, B and c found as

$$(\boldsymbol{A}, \boldsymbol{B}, \boldsymbol{c}) = \arg\min_{(\boldsymbol{\alpha}, \boldsymbol{\beta}, \boldsymbol{\gamma})} \sum_{k=1}^{N} ||\boldsymbol{R}_{c2}(\boldsymbol{x}^{k}) - \boldsymbol{R}_{c1}(\boldsymbol{x}^{k}, \boldsymbol{\alpha}, \boldsymbol{\beta}, \boldsymbol{\gamma})|| \quad (6)$$

while $\boldsymbol{x}^k, k = 1, 2, \dots, N$, are base points, e.g., the so-called star-distribution [6] with center at an optimal solution x_{c1}^* of the model \mathbf{R}_{c1} , i.e., $\mathbf{x}_{c1}^* = \mathbf{a}rg\min\{\mathbf{x}: U(\mathbf{R}_{c1}(\mathbf{x}))\}$. Typically, the number N of base points is between n+1 to 2n+1 with n being the number of design variables. Optionally, in order to find a better starting point for SM optimization, one can perform one or more SM iterations using R_{c1} as a coarse model and R_{c2} as a fine model and use the optimization outcome as a center of the base set in (6). In practice, we often use one of the special cases of model (5). If necessary, model (5) can be enhanced by other mappings, e.g., a frequency scaling [6].

 R_c defined by (5) and (6) is as cheap as R_{c1} , and, at the same time, almost as accurate as R_{c2} in the region determined by the base points x^k . As all coarse models are assumed to be physicsbased, we expect a good global matching between R_{c1} and R_{c2} .

Our algorithm flow can be described as follows:

- Step 1) optimize \mathbf{R}_{c1} to find $\mathbf{x}_{c1}^* = \arg \min\{x\}$ $U(\mathbf{R}_{c1}(\mathbf{x}))$;
- Step 2) choose a base set $\boldsymbol{x}^k, k = 1, \dots, N$;
- Step 3) evaluate \mathbf{R}_{c2} at base points $\mathbf{x}^k, k = 1, \dots, N$;
- Step 4) obtain R_c through parameter extraction (6);
- Step 5) find $\boldsymbol{x}^{(0)} = \arg\min\{\boldsymbol{x}: U(\boldsymbol{R}_c(\boldsymbol{x}))\};$
- Step 6) set i = 0;
- Step 7) evaluate the fine model to find $R_f(x^{(i)})$;
- Step 8) obtain the surrogate model $\mathbf{R}_{s}^{(i)}$ using (3) and (4); Step 9) given $\mathbf{x}^{(i)}$ and $\mathbf{R}_{s}^{(i)}$, obtain $\mathbf{x}^{(i+1)}$ using (2);
- Step 10) if the termination condition is not satisfied set i =i + 1 and go to Step 7); else END.

The algorithm is terminated in the case of convergence or exceeding the user-defined number of iterations. The SM used in (3)–(6) may be of the same or different type, depending on the specifics of R_{c1} , R_{c2} , and R_{f} .

III. EXAMPLES

Consider the third-order Chebyshev bandpass filter [7] shown in Fig. 1. The design parameters are $\boldsymbol{x} = [L_1 L_2 S_1 S_2]^T$ mm.



Fig. 2. Coarse model R_{c1} of the third-order Chebyshev filter (Agilent ADS).

TABLE I **RESULTS FOR THIRD-ORDER CHEBYSHEV MICROSTRIP FILTER**



Fig. 3. Third-order Chebyshev filter: fine model R_f response (solid line), coarse model R_{c1} response (dotted line), and enhanced coarse model R_c response (dashed line) at x_{c1}^* .

Other parameters are: $W_1 = W_2 = 0.4$ mm. The fine model R_f is simulated in Sonnetem [8] with a fine grid of 0.2 mm imes 0.02 mm. The simulation time for R_f is about 25 min. The design specifications are $|S_{21}| \ge -3$ dB for 1.8 GHz $\leq \omega \leq 2.2$ GHz, and $|S_{21}| \leq -20$ dB for 1.0 GHz $\leq \omega \leq 1.6$ and 2.4 GHz $\leq \omega \leq$ 3.0 GHz. R_{c1} is the circuit model implemented in Agilent ADS [9] (Fig. 2). The evaluation time is about 1.5 s. R_{c2} is simulated in Sonnet em, however, with a coarse grid of 2 mm \times 0.1 mm. The simulation time is about 1 min. R_{c2} can not be directly used in the SM optimization because it is too expensive and available only on a coarse grid.

The filter in Fig. 1 was optimized using the standard SM with coarse model R_{c1} as well as with the new multicoarse-model SM approach. The enhanced R_c has been created using R_{c1} , R_{c2} as described in Section II with input and frequency SM and the star-distribution base set (nine evaluations of model R_{c2}). The evaluation time for R_c is virtually the same as for R_{c1} , i.e., 1.5 s. SM optimization used the input SM surrogate $R_s(x) =$ $R_c(\boldsymbol{x} + \boldsymbol{c})$ enhanced by frequency SM [6].

Table I shows that the multicoarse-model SM produces a better solution than the standard SM with a smaller number of fine model evaluations. Fig. 3 shows the responses of R_f, R_{c1} and R_c at the optimal solution of R_{c1} , $\mathbf{x}_{c1}^* = [14.6 \ 15.2 \ 0.56 \ 0.54]^T$, and indicates that the model \mathbf{R}_c provides a better match to the fine model than \mathbf{R}_{c1} , which explains the better performance of the SM algorithm using model R_c . Fig. 4 shows the R_f response at the final solution $\mathbf{x}^* = [14.8 \ 14.8 \ 0.40 \ 0.84]^T$ found by the new algorithm.



Fig. 4. Third-order Chebyshev filter: final fine model response at the solution obtained with the multicoarse-model SM algorithm.



Fig. 5. Open-loop ring resonator bandpass filter [10].



Fig. 6. Coarse model R_{c1} of the open-loop ring resonator filter (Agilent ADS).

Our second example is the open-loop ring resonator bandpass filter [10] shown in Fig. 5. The design parameters are $\boldsymbol{x} = [L_1L_2 \ L_3 \ L_4 \ S_1 \ S_2 \ g]^T$ mm. Other parameter values are: W = 0.6 mm, $W_1 = 0.4$ mm. \boldsymbol{R}_f is simulated in FEKO [11] with a fine mesh. The simulation time for \boldsymbol{R}_f is about 15 min. The design specifications are $|S_{21}| \ge -3$ dB for 2.8 GHz $\le \omega \le$ 3.2 GHz, and $|S_{21}| \le -20$ dB for 1.5 GHz $\le \omega \le 2.5$ GHz and 3.5 GHz $\le \omega \le 4.5$ GHz. \boldsymbol{R}_{c1} is the circuit model implemented in Agilent ADS [9] (Fig. 6). The evaluation time is about 1.5 s. \boldsymbol{R}_{c2} is simulated in FEKO, however, with a coarse mesh. The simulation time is 90 s.

We optimized the filter in Fig. 5 using the standard SM with coarse model R_{c1} as well as the new multicoarse-model SM approach with both R_{c1} and R_{c2} . The enhanced model R_c has been created using the R_{c1} and R_{c2} with input and frequency SM and random base set (eight evaluations of model R_{c2}). Evaluation time for R_c is almost the same as for R_{c1} , i.e., 1.5 s. SM optimization used the input SM surrogate $R_s(x) = R_c(Bx)$ enhanced by frequency SM. Table II shows that the multicoarse-model SM algorithms produce a better solution than the standard SM with a smaller number of fine model evaluations. Fig. 7 shows the fine model response at the final solution $x^* = [25.07 \ 11.32 \ 5.99 \ 4.10 \ 0.24 \ 0.10 \ 0.89]^T$.



Fig. 7. Open-loop ring resonator bandpass filter: final fine model response at the solution obtained with the multicoarse-model SM algorithm.

 TABLE II

 Results for Open-Loop Ring Resonator Filter

Algorithm	Final Specification Error	Number of Fine Model Evaluations [*]
Standard SM algorithm with coarse model R _{c1}	-0.6 dB	8
Multi-coarse-model SM algorithm with models R _{c1} and R _{c2}	-0.9 dB	4
* Excludes fine model evaluation at the starting point		

IV. CONCLUSION

A multicoarse-model SM optimization algorithm is presented. The new technique allows us to improve the quality of SM optimization and reduce its computational cost. The robustness of the method is demonstrated through microwave design optimization examples.

REFERENCES

- [1] J. W. Bandler, Q. S. Cheng, S. A. Dakroury, A. S. Mohamed, M. H. Bakr, K. Madsen, and J. Søndergaard, "Space mapping: The state of the art," *IEEE Trans. Microw. Theory Tech.*, vol. 52, no. 1, pp. 337–361, Jan. 2004.
- [2] S. Koziel, J. W. Bandler, and K. Madsen, "A space mapping framework for engineering optimization: Theory and implementation," *IEEE Trans. Microw. Theory Tech.*, vol. 54, no. 10, pp. 3721–3730, Oct. 2007.
- [3] J. V. Morro, H. Esteban, V. E. Boria, C. Bachiller, and A. Coves, "New multimodel ASM technique for the efficient design of complex microwave circuits," in *IEEE MTT-S Int. Dig.*, Long Beach, CA, 2005, pp. 1613–1616.
- [4] K. L. Wu, Y. J. Zhao, J. Wang, and M. K. K. Cheng, "An effective dynamic coarse model for optimization design of LTCC RF circuits with aggressive space mapping," *IEEE Trans. Microw. Theory Tech.*, vol. 52, no. 1, pp. 393–402, Jan. 2004.
- [5] S. Koziel and J. W. Bandler, "Interpolated coarse models for microwave design optimization with space-mapping," *IEEE Trans. Microw. Theory Tech.*, vol. 55, no. 8, pp. 1739–1746, Aug. 2007.
- [6] S. Koziel, J. W. Bandler, A. S. Mohamed, and K. Madsen, "Enhanced surrogate models for statistical design exploiting space mapping technology," in *IEEE MTT-S Int. Dig.*, Long Beach, CA, Jun. 2005, pp. 1609–1612.
- [7] J. T. Kuo, S. P. Chen, and M. Jiang, "Parallel-coupled microstrip filters with over-coupled end stages for suppression of spurious responses," *IEEE Microw. Wireless Compon. Lett.*, vol. 13, no. 10, pp. 440–442, Oct. 2003.
- [8] emTM version 10.53. Sonnet Software, Inc., North Syracuse, NY, 2007.
- [9] Agilent ADS, version 2003C. Agilent Technologies, Santa Rosa, CA, 2003.
- [10] C. Y. Chen and C. Y. Hsu, "A simple and effective method for microstrip dual-band filters design," *IEEE Microw. Wireless Compon. Lett.*, vol. 16, no. 5, pp. 246–248, May 2006.
- [11] "FEKO[®] User's Manual" EM Software & Systems—S.A. (Pty), Ltd., 2004 [Online]. Available: http://www.feko.info